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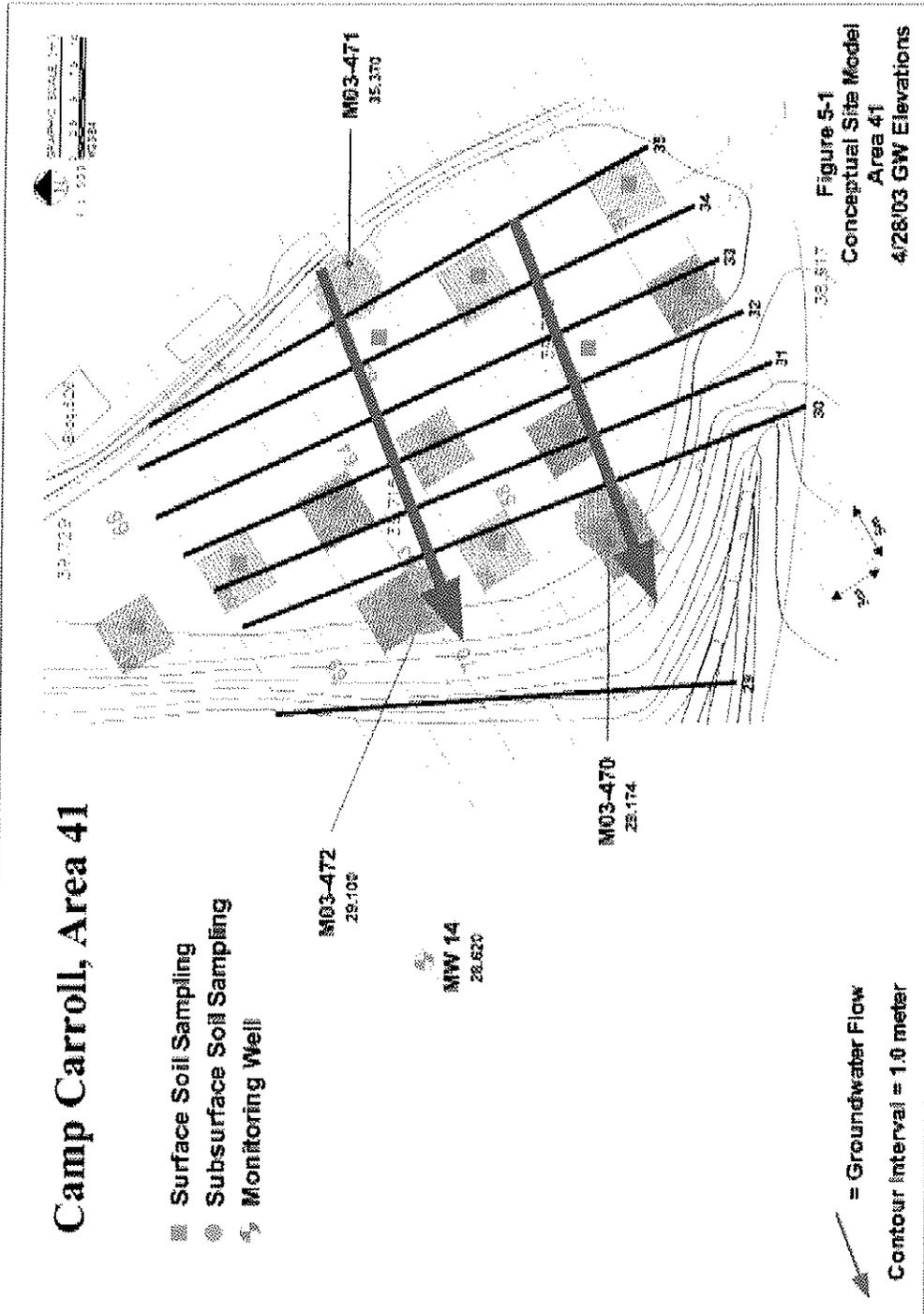
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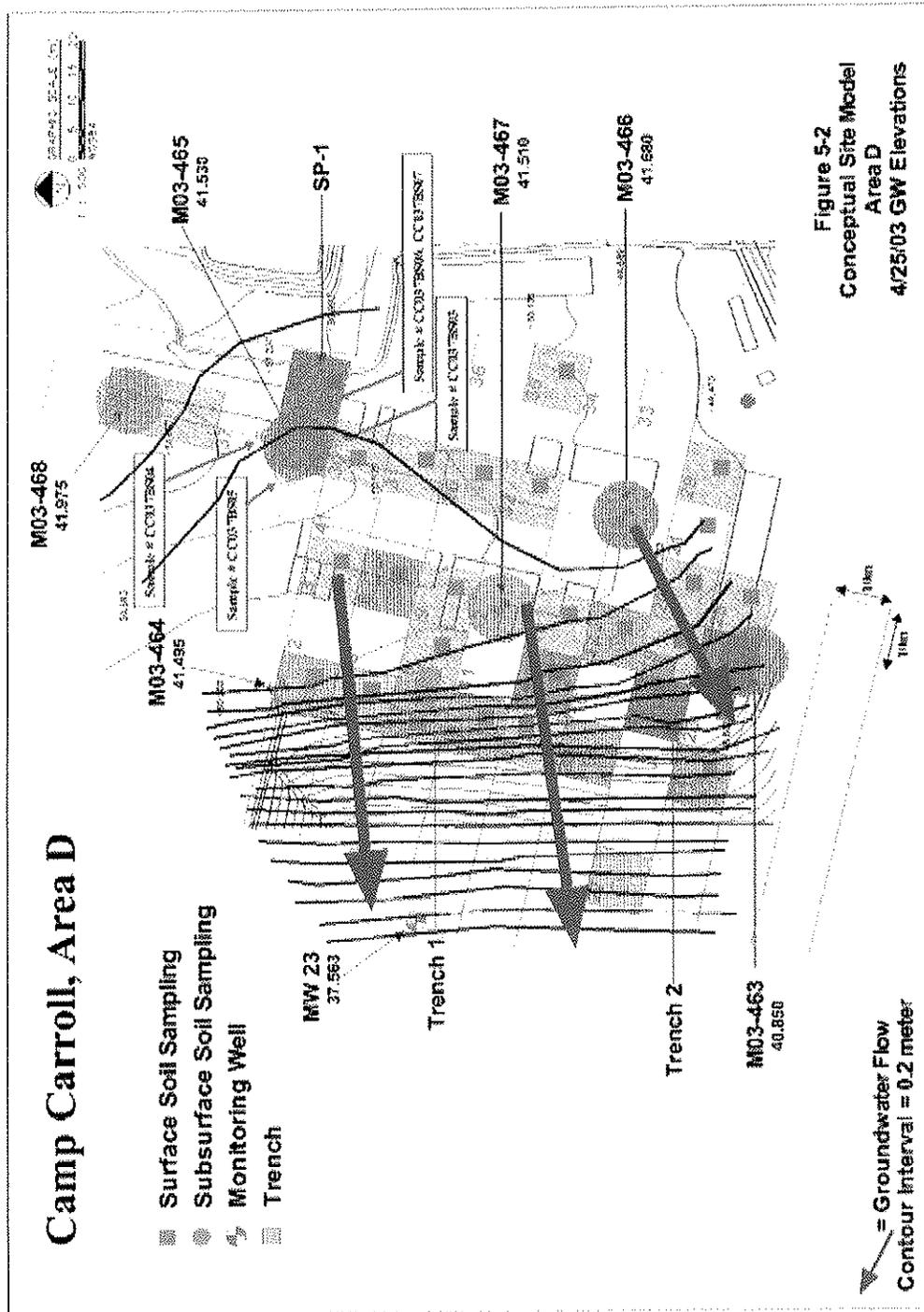
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higher fluid elevations to lower fluid elevations); however, this flow may be disrupted by any non-homogeneous nature of the rock media. During drilling activities, no major fractures or faulting was observed in the soil cores. Thus it is anticipated that groundwater flow beneath the site will be in the general direction of the observed hydraulic gradient.

Groundwater depths have been observed to vary over time at the site, however, the hydraulic gradient and direction of groundwater flow has remained relatively constant over the approximately four month period monitored during the field activities for this project. The observed variations in water table elevation are presumed to result from large quantities of infiltrated rainwater during storm events and seasonal periods of higher precipitation. The reasonably low storage capacity typical of igneous rock aquifers allows rapid increases in water level with increased rates of recharge.

In general, groundwater level contour maps prepared for each of the sites depict the groundwater gradient and presumed direction of groundwater flow directed towards the west. For illustration purposes, water table maps prepared for April 28, 2003 (Area 41) and April 25, 2003 (Area D) are depicted on the CSMs. These maps represents general ground-water gradient conditions at the Site and show that for each of the two sites, contaminants dissolved in groundwater will travel predominantly to the west. If additional groundwater level information becomes available from other locations within or in the vicinity of the Site, the interpreted groundwater flow patterns may require modification.

The conceptualized movement of groundwater and dissolved contaminants are depicted with directional arrows on the CSMs. It is anticipated that soil-bound contaminants are leaching vertically downward to the groundwater table with infiltrated rainwater. When reaching the groundwater, the dissolved chemicals are migrating laterally with the ground-water at the site. At the location of the observed soil and groundwater contaminant plumes, the groundwater gradient is directed to the west, and dissolved contaminants will travel preferentially in this direction when rock permeability is available with this orientation.

In summary, the identified groundwater gradient at each of the two sites investigated is directed toward the west. It appears that aqueous phase contaminants originating in

shallow soils may have migrated downward through the vadose zone to the groundwater table, and then laterally to the west with groundwater flow. The observed presence of similar contaminants in groundwater wells located to the west of Area 41 (Monitoring Well MW-14) and Area D (Monitoring Well MW-23) are consistent with this scenario.

## 5.2 PRELIMINARY SCREENING EVALUATION

This section documents the results of a Human Health Preliminary Risk Evaluation (PRE) of potential human exposure associated with chemical compounds present at the Camp Carroll Area 41 and Area D sites. The purpose of the PRE is to identify sites that do not warrant further consideration in the site evaluation process and sites that require immediate remedial actions or further studies to address concerns related to elevated concentrations of chemicals in environmental media.

### Approach

The approach for this human health PRE is based on the *USEPA Risk Assessment Guidance for Superfund (RAGS): Volume 1 - Human Health Evaluation Manual (Parts A and B)* (USEPA 1989, 1991). The Risk Assessment process is conducted in two phases. The first phase is the initial conservative screening PRE conducted using USEPA Region 9 PRGs (USEPA 2000). This phase is followed, when necessary, by a site-specific Baseline Risk Assessment. A brief overview of the risk assessment process is presented below.

The initial screening PRE is performed when the complete or potentially complete exposure pathways of concern and pathway-specific exposure parameters are the same as those used in the development of the standards in which they are compared. For this preliminary assessment, the preliminary screening criteria are the United States Forces Korea Environmental Governing Standards (USFK EGS) and the USEPA Region 9 Preliminary Remediation Goals (PRGs) (USEPA 2000). USFK EGS drinking water MCLs are applicable to sites in which groundwater is used as a drinking water source. PRGs are health-based remediation goals developed by USEPA Region 9 for soil, groundwater, and ambient air. USEPA Region 9 has developed soil PRGs for both residential and industrial land use scenarios. If pathways not addressed in the PRGs or USFK EGS are complete or potentially complete at the Site, or if site-specific exposure factors differ from those used in the development of the PRGs or USFK EGS, a

site-specific baseline risk assessment may be performed. Additionally, if the conservative screening PRE results indicate potentially significant health risks, a site-specific baseline risk assessment is performed to derive more realistic risk estimates.

As stated above, the use of screening values for estimating human health risks requires that the exposure pathways and exposure assumptions used in the development of PRGs or USFK EGS are consistent with the exposure pathways and exposure assumptions for the Site. In using PRGs or USFK EGSs to estimate potential health risks, the screening PRE essentially adopts the exposure pathways and exposure parameter values used to develop the standards. Therefore, the screening PRE does not use any site-specific information, other than media chemical concentration data. The underlying assumptions used in the development of PRGs or USFK EGSs relevant to the Camp Carroll Site are summarized below:

PRG Exposure Pathways – Industrial Land Use Soil Media

- Incidental ingestion
- Inhalation of particulates
- Inhalation of volatile compounds
- Dermal absorption

Exposure Pathways – Industrial Land Use Groundwater Media

- Incidental ingestion

The exposure parameters used to develop Region 9 Industrial Soil PRGs are presented below.

PRG Exposure Parameter Values – Industrial Land Use – Soil

• Target cancer risk	1E-06 (unitless)
• Target hazard quotient	1 (unitless)
• Adult worker body weight	70 kg
• Exposed adult skin surface area	3,300 cm <sup>2</sup> /day
• Adult worker soil adherence factor	0.2 mg/cm <sup>2</sup>
• Dermal absorption factor in soil (svocs)	0.10 (unitless)
• Adult worker respiration (inhalation) rate	20 m <sup>3</sup> /day
• Adult worker soil ingestion rate	100 mg/day
• Exposure frequency	250 days/year
• Exposure duration adult	25 years
• Lifetime	70 years
• Volatilization factor for soil	Chemical-specific
• Particulate emission factor	1.3E+09 (unitless)

## **Methodology**

The steps involved in performing a screening PRE are as follows:

- identification of relevant data sets and chemicals of potential concern
- exposure pathways analysis and development of a conceptual evaluation model (CEM)
- estimation of exposure point concentrations (EPCs)
- calculation of screening cumulative health risks
- evaluation of health effects posed by lead, if necessary
- evaluation of the screening PRE results

### Identification of Relevant Data Sets and Chemicals of Potential Concern

Before performing a screening PRE, a review of the analytical data is performed to identify the appropriate impacted area(s) of concern and to develop an understanding of three-dimensional contaminant distributions. If environmental samples are analyzed for a chemical using more than one analytical method, the most reliable results (as indicated by data validation qualifiers or laboratory data qualifiers) that provide representative environmental concentrations are selected. To conservatively protect human health, the screening PRE focuses on data from the impacted area(s) within the study Site. Chemicals not included in the screening PRE are compounds that are not regulated under the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) and contaminants that do not have available USFK EGS or USEPA Region 9 PRGs.

### Exposure Pathways Analysis and Development of a CEM

In accordance with USEPA (1989), human health PREs are intended to address only contaminants for which there is a complete or potentially complete exposure pathway under current and future land use conditions. The first step in the exposure pathway analysis is the identification of possible human receptors. The identification of possible human receptors considers both current and future land uses of the Site and may include

adult and child residents, workers, recreators, trespassers, and other receptors as appropriate. Relevant exposure pathways are then evaluated to determine their completeness based on receptor characteristics, fate and transport considerations, the types of chemicals detected in site media, and other site-specific factors.

An exposure pathway consists of four distinct elements: (1) a source and mechanism of release, (2) a retention medium or transport mechanism, (3) a point of potential contact with a receptor, and (4) an exposure route (USEPA 1989). Each of these four elements must be present for a given exposure pathway in order for the pathway to be complete. In the absence of a complete exposure pathway, there is no exposure and consequently no risk to human health. The purpose of the exposure pathways analysis is to evaluate whether a possible exposure pathway is complete, potentially complete, incomplete, or insignificant. A potentially complete exposure pathway is one that either could be complete in the future if certain conditions are met, or could be complete under current conditions if certain conditions are present but for which data are inadequate for making a definitive determination. Potentially complete exposure pathways are addressed in the PRE in the same manner as complete exposure pathways. An exposure pathway may be complete, but insignificant, if the degree of exposure is found to be insignificant as compared to other exposure pathways. Risks are generally not estimated for insignificant exposure pathways.

#### Estimation of Exposure Point Concentrations

Exposure point concentrations are defined by USEPA as the chemical concentrations a receptor may contact at a location over the exposure period (USEPA 1989). Exposure point concentrations may be estimated using direct measurement data (i.e., soil concentrations from the sampling and analytical programs) or a combination of direct measurement data as well as fate and transport modeling results. Direct measurement data are appropriately used when there is human contact with the media sampled, such as ingestion of or dermal contact with soil or groundwater. For these direct contact pathways, site-specific measured chemical concentrations are used to estimate exposure point concentrations. For pathways where exposure points are spatially separate from the media sampled, or where contact media are not sampled, fate and transport modeling is used in conjunction with site-specific direct measurement data to estimate exposure point

concentrations. Examples of this method include estimating onsite (or offsite) chemical concentrations in air or groundwater from onsite soil data.

#### Calculation of Screening Cumulative Health Risks for Soil

Potential health risks are calculated using reasonable maximum exposure (RME) point concentrations, chemical-specific cancer and noncancer PRGs, and the cancer and noncancer target risk values. Since the USEPA Region 9 PRGs are defined as the concentrations of chemicals in environmental media that correspond to an excess cancer risk of one-in-one-million (1E-06) or a noncancer hazard index (HI) of 1, the cancer and noncancer target risk values are 1E-06 and 1, respectively. As illustrated in the following equations, potential excess cancer risks and noncancer HIs for each chemical detected in each media at the Site are estimated using the ratio of the exposure point concentration and the carcinogenic or noncarcinogenic PRG, respectively.

For noncancer risk, the hazard index is calculated as:

$$HI = \frac{EPC}{PRG_{nc}}$$

Where,

HI = Hazard Index (unitless)

EPC = Exposure Point Concentration (mg/kg)

PRG<sub>nc</sub> = Preliminary Remediation Goal based on noncancer effects

The estimated excess cancer risk is calculated as:

$$Risk = TR \left( \frac{EPC}{PRG_c} \right)$$

Where,

Risk – Excess Cancer Risk (unitless)

TR = Target Risk Level upon which the PRG is based ( $1 \times 10^{-6}$ )

EPC = Exposure Point Concentration (mg/kg)

PRGc = Preliminary Remediation Goal based on cancer (mg/kg)

Assuming that the effects posed by different contaminants are additive (i.e., that no synergistic or antagonistic interactions occur) and that chemical concentrations and other exposure parameters remain constant throughout the exposure period (USEPA 1989), cumulative excess cancer risks and HIs are estimated by adding the contributions from each chemical. Thus, the cumulative excess cancer risk for the Site is the sum of the estimated excess cancer risks for each chemical, and the cumulative HI for the Site is the sum of the estimated HIs for each chemical.

#### Evaluation of Health Effects Posed by Lead in Soil

Because there is no discernible, safe threshold for lead exposure, an HI for lead cannot be determined by employing the approach used for other chemicals. Thus, the cumulative HI reported in the screening PRE does not include a quantitative HI estimate for lead. Lead is evaluated separately in the screening PRE by direct comparison to USEPA Region 9 PRGs. USEPA Region 9 currently proposes an industrial PRG for lead of 750 mg/kg in soil.

#### Evaluation of the Screening PRE Results

The human health PRE decision tree for all chemicals except lead is described below.

1. If the site has been adequately characterized:

- No further action is recommended when the cumulative excess cancer risk based on the maximum detected concentration is less than or equal to  $1E-06$  and the HI is less than or equal to 1, and if there are no adverse ecological impacts.

- A site-specific baseline risk assessment is performed when the screening cumulative excess cancer risk based on the maximum detected concentration is greater than  $1E-06$  and/or the HI is greater than 1.

- For lead, a site-specific risk assessment may be performed if maximum and/or RME lead concentrations are greater than USEPA Region 9 PRGs.

In other cases, it may be determined that additional data are needed in order to better evaluate the site.

### **5.2.1 SCREENING HUMAN HEALTH PRE FOR THE CAMP CARROLL SITE**

This screening human health PRE was performed to assess potential human health risks if remedial actions are not taken at the Camp Carroll Site.

#### **Development of a Conceptual Evaluation Model (CEM)**

A CEM describes the interrelationships between all potential receptors, exposure points, transport pathways and contaminant sources at a site. Development of a site-specific CEM and determination of relevant potential exposure pathways evaluated in the PRE must consider historical and current site use as well as potential future land use conditions.

#### Historical and Current Land Use Conditions

A detailed description of past and current operations at Camp Carroll is provided in Section 1.

#### Future Land Use Conditions

Use of both the Area 41 and Area D sites are proposed to remain industrial in the future. The water table aquifer will continue to be a nonpotable water supply.

#### CEM Development and Exposure Pathways Analysis

Based on sources of contaminants at the Camp Carroll Site, possible complete or potentially complete exposure pathways associated with soils include incidental ingestion of and dermal contact; incidental ingestion, dermal contact, and inhalation of soil-derived

fugitive dusts; inhalation of volatile compounds in soils. The complete and potentially complete exposure pathways identified in this analysis for soil are consistent with those used by USEPA to develop PRGs. Therefore, use of PRGs for estimating soil exposure risks is appropriate.

Potentially complete exposure pathways between groundwater and human receptors exist via the ingestion or dermal contact with groundwater during industrial activities and through the inhalation of chemicals that may volatilize to air. Only the drinking water pathway has been evaluated in this PRE. Other pathways may be evaluated in site-specific baseline risk assessment if deemed appropriate.

Other potential exposure pathways not included in this PRE are the consumption of fish, beef or other livestock that may have been impacted by the site, ingestion of fruits or vegetables grown on the site, migration of contaminants to an underlying potable aquifer, inhalation of volatiles that may have migrated into building and ecological pathways. Based on the results of the screening PRE, these potential pathways may be recommended for evaluation in a comprehensive baseline risk assessment or ecological risk assessment.

#### **Identification of Relevant Datasets**

This study is focused on the nature and extent of target COPCs for the impacted soil and groundwater at the Site. Soil and groundwater at the Site were analyzed for VOCs, SVOCs, metals, dioxins and furans (dioxins), chlorinated pesticides and total petroleum hydrocarbons (TPH). The complete list of chemicals analyzed is provided in Table 5-1. All surface soil samples, subsurface soil samples and groundwater samples were collected from within the geographic boundaries of the Site. Soil samples were limited to "open" areas within the study boundary. "Open" areas within the study boundary are defined as any area, paved or unpaved, that were readily accessible to field personnel and sampling equipment. Groundwater was sampled from monitoring wells within the study boundary. All analytical data collected during the Site assessment were evaluated for inclusion in the PRE. TPH and petroleum hydrocarbon fractions were not evaluated using Region 9 PRGs because PRGs have not been published for these chemical groups. However, available TPH data, was compared to Hawaii State TOALs. TOALs are not risk-based values, but are remediation level goals endorsed by the State of Hawaii. It is

important to note that TOALs are not *de facto* cleanup standards and do not have to be applied as such. TOALs are helpful in providing long-term targets to use during the analysis of different remedial activities. If TPH values onsite exceed State of Hawaii TOALs, a site-specific risk analysis may be conducted to determine potential health risks.

Because Area 41 and Area D were historically used for different purposes and the levels of chemicals in soil and groundwater may differ, the Screening PRE has evaluated the two sites separately. Comparison of analytical soil data with USEPA Region 9 PRGs for Area 41 and Area D sites are provided in Tables 5-2 and 5-3. Groundwater comparison with USFK EGS for Area 41 and Area D sites are provided in Tables 5-4 and 5-5.

#### **Methodology for Determining EPCs**

For the Camp Carroll PRE, the maximum detected concentration was deemed appropriate for use as the RME concentration. The RME is a conservative estimate of exposure and when used to calculate potential health risks, are protective of the high end of the population distribution (USEPA 1989, USEPA 1992a).

#### **5.2.2 Screening PRE Results**

##### **Soil Results**

In the screening PRE, cumulative risks were estimated using the RME point concentration (maximum concentration detected) and USEPA Region 9 PRGs. Results are shown in Tables 5-2 and 5-3. PRGs are not directly applicable to subsurface soil data, however, for the purposes of the screening PRE, surface and subsurface soil data were conservatively evaluated as a single dataset. In this discussion, the term "risk drivers" is used to refer to chemicals with concentrations exceeding their respective industrial soil PRGs and contribute approximately 10 percent or more of the cumulative excess cancer risk or HI. Since there are no differences in the screening PRE approaches for current and future industrial workers, the scenario evaluated is referred to as "current and future industrial land use."

##### Current and Future Industrial land Use

For soil, the cumulative excess cancer risk and HI based on the RME exposure point concentration for Area 41 are 2E-05 and 4.2E-02, respectively, as shown in Table 5-2.

Cumulative excess cancer risk and HI for Area D are 2E-05 and 5.7E-01, respectively, as shown in Table 5-3. The excess cancer risks for both areas are greater than the point-of-departure risk of 1E-06, but within the USEPA upper bound acceptable cancer risk level of 1E-04. The HIs are less than the target value of 1.

Carcinogenic risk drivers for Area 41 are arsenic, Dieldrin, 4,4'-DDD, 4,4'-DDT, gamma-Chlordane, and Benzo(a)pyrene. Carcinogenic risk drivers for Area D are arsenic, 4,4'-DDT, and Trichloroethene. The above screening PRE results do not include the health risk due to lead exposure. The RME lead concentration detected in soil at Area 41 and Area D are 38 and 48.3 mg/kg, respectively. Lead concentrations detected in surface and subsurface soils are less than the USEPA Region IX industrial soil PRG of 750 mg/kg.

**Table 5-1  
 Analyte List  
 Camp Carroll Area 41 and Area D**

Compound	Soil	Groundwater
<b>METALS</b>		
Arsenic	X	X
Barium	X	X
Cadmium	X	
Chromium	X	X
Lead	X	X
Mercury	X	X
Selenium	X	X
Silver	X	X
<b>CHLORINATED PESTICIDES</b>		
alpha-BHC	X	X
beta-BHC	X	X
delta-BHC	X	X
gamma-BHC (Lindane)	X	X
Hepatochlor	X	X
Aldrin	X	
Hepatochlor epoxide	X	
Endosulfan I	X	
Dieldrin	X	X
4,4'-DDE	X	
Endrin	X	
Endosulfan II	X	
4,4'-DDD	X	
Endosulfan sulfate	X	
4,4'-DDT	X	
Methoxychlor	X	
Endrin Ketone	X	
Endrin Aldehyde	X	
alpha-Chlordane		X
gamma-Chlordane	X	
<b>VOCS/SVOCs</b>		
1,2,3-Trichlorobenzene	X	
2-Chlorotoluene	X	X
4-Chlorotoluene	X	X
Chlorobenzene	X	X
cis-1,2-Dichloroethene	X	X
trans-1,2-Dichloroethene		X
Tetrachloroethene	X	X
Toluene	X	X
Trichloroethene	X	X
2-Methynaphthalene	X	X
2-Methylphenol (o-Cresol)	X	X

Compound	Soil	Groundwater
3&4-Methylphenol (p&m-Cresol)	X	X
Benzo(a)anthracene	X	
Benzo(a)pyrene	X	
Benzo(b)fluoranthene	X	
Benzo(g,h,i)perylene	X	
bis(2-Ethylhexyl)phthalate	X	
Chrysene	X	
Fluoranthene	X	X
Indeno(1,2,3-cd)pyrene	X	
Phenanthrene	X	
Pyrene	X	
1,1,1,2-Tetrachloroethane		X
1,1,2,2-Tetrachloroethane		X
1,1,2-Trichloroethane		X
1,1-Dichloroethane		X
1,1-Dichloroethene		X
1,2,4-Trimethylbenzene		X
1,3,5-Trimethylbenzene		X
1,4-Dichlorobenzene		X
Acetone		X
Benzene		X
Carbon disulfide		X
Chloroethane		X
Chloroform		X
Ethylbenzene		X
Isopropylbenzene (Cumene)		X
Methylene chloride		X
Naphthalene		X
n-Propylbenzene		X
o-Xylene		X
P & M -Xylene		X
Vinyl chloride		X
1,4-Dichlorobenzene		X
Acenaphthene		X
Benzyl alcohol		X
Butylbenzylphthalate		X
Diethylphthalate		X
Napthalene		X
Phenol		X
<b>DIOXINS/FURANS</b>		
Total TEQ	X	X
<b>TOTAL PETROLEUM HYDROCARBONS</b>		
Gasoline Range	X	X
Diesel Range	X	X
Oil Range	X	

**Table 5-2**  
**PRG Screening and COPC Selection**  
**Current Industrial - Surface Soil Exposure Pathway**  
**Camp Carroll Area 41**

Compound	PRG <sub>ca</sub> (mg/kg)	PRG <sub>nc</sub> (mg/kg)	RME Concentration (mg/kg)						
			EPC	> PRG <sub>ca</sub> ?	> PRG <sub>nc</sub> ?	ECR	%	HI	%
<b>METALS</b>									
Arsenic	1.6E+00	2.6E+02	8.24E+00	YES	No	5 E-06	21	3.2E-02	75
Barium	-	6.7E+04	2.35E+02	No	No			3.5E-03	8
Cadmium	-	4.5E+02	5.86E-01	No	No			1.3E-03	3
Chromium	4.5E+02	-	7.99E+01	No	No	2 E-07	<1		
Lead	-	7.5E+02	3.80E+01	No	No				
Mercury	-	6.2E+01	1.28E-02	No	No			2.1E-04	<1
Selenium	-	5.1E+03	4.44E-01	No	No			8.7E-05	<1
Silver	-	5.1E+03	5.60E-02	No	No			1.1E-05	<1
<b>CHLORINATED PESTICIDES</b>									
alpha-BHC	3.6E-01	-	8.04E-04	No	No	2 E-09	<1		
beta-BHC	1.3E+00	-	4.79E-03	No	No	4 E-09	<1		
delta-BHC	-	-	8.56E-01	No	No				
gamma-BHC (Lindane)	1.7E+00	-	3.90E-03	No	No	2 E-09	<1		
Hepatochlor	3.8E-01	-	3.48E-03	No	No	9 E-09	<1		
Aldrin	1.0E-01	-	1.54E-02	No	No	2 E-07	<1		
Hepatochlor epoxide	1.9E-01	-	1.05E-02	No	No	6 E-08	<1		
Endosulfan I	-	3.7E+03	8.44E-02	No	No			2.3E-05	<1
Dieldrin	1.1E-01	-	5.01E-01	YES	No	5 E-06	19		
4,4'-DDE	7.0E+00	-	2.65E+00	No	No	4 E-07	2		
Endrin	-	1.8E+02	3.69E-02	No	No			2.1E-04	<1
Endosulfan II	-	3.7E+03	2.07E-03	No	No			5.0E-07	<1
4,4'-DDD	1.0E+01	-	2.17E+01	YES	No	2 E-06	9		
Endosulfan sulfate	-	3.7E+03	1.46E-01	No	No			3.9E-05	
4,4'-DDT	7.0E+00	-	4.30E+01	YES	No	6 E-06	25		
Methoxychlor	-	3.1E+03	6.63E-03	No	No			2.1E-06	<1
Endrin Ketone	-	1.8E+02	1.21E-01	No	No			6.7E-04	2
Endrin Aldehyde	-	1.8E+02	2.88E-03	No	No			1.6E-05	<1
gamma-Chlordane	6.5E+00	-	8.50E+00	YES	No	1 E-06	5		
<b>VOCS/SVOCs</b>									
1,2,3-Trichlorobenzene	-	3.0E+03	1.93E-02	No	No			6.4E-06	<1
2-Chlorotoluene	-	5.6E+02	1.93E-02	No	No			3.4E-05	<1
4-Chlorotoluene	-	5.6E+02	1.93E-02	No	No			3.4E-05	<1
Chlorobenzene	-	5.3E+02	1.93E-02	No	No			3.6E-05	<1
cis-1,2-Dichloroethene	-	1.5E+02	1.93E-02	No	No			1.3E-04	<1
Tetrachloroethene	3.4E+00	-	5.02E-01	No	No	1 E-07	<1		
Toluene	-	5.2E+02	8.75E-02	No	No			1.7E-04	<1
Trichloroethene	1.1E-01	-	1.54E-02	No	No	1 E-07	<1		

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Results Table 5-3

**Table 5-3  
PRG Screening and COPC Selection  
Current Industrial - Surface Soil Exposure Pathway  
Camp Carol Area D**

Compound	PRG <sub>ca</sub> (mg/kg)	PRG <sub>nc</sub> (mg/kg)	RME Concentration (mg/kg)						
			EPC	> PRG <sub>ca</sub> ?	> PRG <sub>nc</sub> ?	ECR	%	HI	%
<b>METALS</b>									
Arsenic	1.6E+00	2.6E+02	2.07E+01	YES	No	1 E-05	61	8.0E-02	14
Barium	-	6.7E+04	2.11E+02	No	No			3.1E-03	<1
Cadmium	-	4.5E+02	2.87E+00	No	No			6.4E-03	1
Chromium	4.5E+02	-	1.56E+01	No	No	3 E-08	<1		
Lead	-	7.5E+02	4.83E+01	No	No				
Mercury	-	6.2E+01	1.46E-02	No	No			2.4E-04	<1
Selenium	-	5.1E+03	3.85E-01	No	No			7.5E-05	<1
Silver	-	5.1E+03	4.72E-01	No	No			9.3E-05	<1
<b>CHLORINATED PESTICIDES</b>									
alpha-BHC	3.6E-01	-	1.65E-03	No	No	5 E-09	<1		
beta-BHC	1.3E+00	-	2.52E-03	No	No	2 E-09	<1		
delta-BHC	-	-	1.93E-03	No	No				
gamma-BHC (Lindane)	1.7E+00	-	3.91E-02	No	No	2 E-08	<1		
Hepatochlor	3.8E-01	-	1.10E-01	No	No	3 E-07	1		
Aldrin	1.0E-01	-	8.82E-04	No	No	9 E-09	<1		
Hepatochlor epoxide	1.9E-01	-	1.10E-01	No	No	6 E-07	3		
Endosulfan I	-	3.7E+03	8.00E-02	No	No			2.2E-05	<1
Dieldrin	1.1E-01	-	5.11E-03	No	No	5 E-08	<1		
4,4' DDE	7.0E+00	-	4.82E 02	No	No	7 E 00	<1		
Endrin	-	1.8E+02	1.10E-01	No	No			6.1E-04	<1
Endosulfan II	-	3.7E+03	1.46E-03	No	No			3.9E-07	<1
4,4'-DDD	1.0E+01	-	5.16E-01	No	No	5 E-08	<1		
Endosulfan sulfate	-	3.7E+03	1.10E-01	No	No			3.0E-05	<1
4,4'-DDT	7.0E+00	-	2.93E+01	YES	No	4 E-06	20		
Methoxychlor	-	3.1E+03	1.10E-01	No	No			3.5E-05	<1
Endrin Ketone	-	1.8E+02	1.10E-01	No	No			6.1E-04	<1
Endrin Aldehyde	-	1.8E+02	1.10E-01	No	No			6.1E-04	<1
gamma-Chlordane	6.5E+00	-	3.33E-03	No	No	5 E-10	<1		
<b>VOCS/SVOCs</b>									
1,2,3-Trichlorobenzene	-	3.0E+03	3.47E-02	No	No			1.2E-05	<1
2-Chlorotoluene	-	5.6E+02	5.28E-01	No	No			9.4E-04	<1
4-Chlorotoluene	-	5.6E+02	1.93E+00	No	No			3.4E-03	<1
Chlorobenzene	-	5.3E+02	6.10E-02	No	No			1.2E-04	<1
cis-1,2-Dichloroethene	-	1.5E+02	2.04E-01	No	No			1.4E-03	<1
Tetrachloroethene	3.4E+00	-	2.00E+00	No	No	6 E-07	3		

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### Groundwater Results

The following table summarizes the results for Area 41 groundwater samples that exceeded EGS screening criteria. USFK EGS values are analogous to United States MCLs. Exceedances in the EGS require remedial actions if groundwater is to be used as a drinking water source.

Sample ID	Analyte	Conc. (mg/L)	EGS (mg/L)
CC053WS01	tetrachloroethene	0.192	0.005
CC054WS01	tetrachloroethene	11.1	0.005
CC066WS01	tetrachloroethene	0.504	0.005
CCM14WS01	tetrachloroethene	0.0926	0.005
CC053WS01	trichloroethene	0.0237	0.005
CC054WS01	trichloroethene	0.171	0.005
CC066WS01	trichloroethene	0.325	0.005
CCM14WS01	trichloroethene	0.0126	0.005
CC054WS01	1,2-dichloroethene	0.0305	0.005

Notes:  
EGS = USFK Environmental Governing Standards  
mg/L= milligrams per liter

The following table summarizes the results for Area D groundwater samples that exceeded EGS screening criteria.

<b>Table 5-5</b> <b>Summary of EGS Exceedances</b> <b>Area D Groundwater Samples</b>			
Sample ID	Analyte	Conc. (mg/L)	EGS (mg/L)
CC001WS01	tetrachloroethene	0.00888	0.005
CC024WS01	tetrachloroethene	0.423	0.005
CC037WS01	tetrachloroethene	0.35	0.005
CC038WS01	tetrachloroethene	0.0247	0.005
CC039WS01	tetrachloroethene	0.203	0.005
CC137WS01	tetrachloroethene	0.343	0.005
CC237WS01	tetrachloroethene	0.427	0.005
CC024WS01	trichloroethene	0.361	0.005
CC037WS01	trichloroethene	0.949	0.005
CC039WS01	trichloroethene	0.0754	0.005
CC137WS01	trichloroethene	0.941	0.005
CC237WS01	trichloroethene	1.4	0.005
CC012WS01	cis-1,2-dichloroethene	0.00966	0.005
CC024WS01	cis-1,2-dichloroethene	0.386	0.005
CC037WS01	cis-1,2-dichloroethene	1.32	0.005
CC039WS01	cis-1,2-dichloroethene	0.122	0.005
CC137WS01	cis-1,2-dichloroethene	1.21	0.005
CC237WS01	cis-1,2-dichloroethene	1.67	0.005
CCM23WS01	cis-1,2-dichloroethene	0.0105	0.005
CC137WS01	trans-1,2-dichloroethene	0.0398	0.005
CC237WS01	trans-1,2-dichloroethene	0.0376	0.005
CC037WS01	benzene	0.00691	0.005
CC039WS01	benzene	0.014	0.005
CC137WS01	benzene	0.00692	0.005
CC237WS01	benzene	0.00693	0.005
CC012WS01	Lindane	0.114	0.002
CC024WS01	Lindane	8.76	0.002
CC039WS01	Lindane	0.362	0.002
CC024WS01	alpha-Chlordane	0.05	0.002

Notes:

EGS = USFK Environmental Governing Standards

mg/L= milligrams per liter

A review of the above tables indicates detected compound concentrations that exceeded EGS values for groundwater are limited to VOCs and pesticides. A baseline groundwater investigation conducted by Woodward Clyde Consultants (WWC 1992b) reported relatively widespread contamination of the aquifer throughout the base. The most common contaminants identified were the chlorinated solvents trichloroethylene, tetrachloroethylene, and 1,2-dichloroethylene. These contaminants were detected in 15 of 18 groundwater monitoring wells sampled and in 8 of 10 water supply wells sampled during the survey in April 1992. Subsequent detections of chlorinated solvents at the subject sites may reflect the widespread aquifer contamination rather than location-specific impacts. In addition, the widespread surface application of pesticides may result in increased background levels of these compounds.

Monitoring well M03-471 (grid cell 53) is located on the eastern side of Area 41 and was intended to provide background chemical information for this site. The detection of VOCs and dioxins in this well may indicate elevated background concentrations of these compounds in the area.

Monitoring well M03-468 (grid cell 38) is located on the north and eastern side of Area D and was intended to provide background chemical information for this site. The detection of TPH and VOCs in this well may indicate elevated background concentrations of these compounds in the area.

Despite potential elevated background VOC levels, several groundwater samples contained relatively high concentrations of chlorinated solvents that suggest a local source. In particular, sample CC054WS01 obtained from monitoring well M03-470 in Area 41 contained a reported tetrachloroethene concentration of 11.1 mg/L and sample CC237WS01 obtained in monitoring well M03-465 in Area D contained a reported trichloroethene concentration of 1.4 mg/L. Cis-1,2-dichloroethene concentrations were also greater than 1.2 mg/L in monitoring well M03-465 (samples CC037WS01, CC137WS01, and CC237WS01). In addition, sample CC024WS01 in Area D contained the pesticide Lindane with a concentration of 8.76 mg/L.

#### Uncertainty Analysis

Uncertainties in the risk estimates are related primarily to the methodologies and parameter values used in estimating exposure and toxicity in humans. They are also the product of many factors affecting each component of the risk assessment process, namely data collection/evaluation and selection of COPCs, exposure assessment, and toxicity assessment. These factors generally include, at a minimum, measurement errors, conservative exposure and modeling assumptions, and uncertainty and variability of the values used in the assessment. The compounding effects can be at least two orders of magnitude or more. This section presents a qualitative discussion of the uncertainties, assumptions, and limitations as well as the scientific basis and rationale for the PRE.

Uncertainties associated with the exposure assessment in this PRE involve, at a minimum, those associated with the estimation of exposure point concentrations, identification of complete or potentially complete pathways, and use of upper-bound exposure parameters.

Another source of uncertainty in estimating exposures is the assumption that individuals within a particular receptor population (or subpopulation) will receive the same intake doses. Variability in parameters such as absorption rates, ingestion rates, dermal contact rate, skin surface area, frequency and duration of exposure, body weight, and activity pattern will exist even in a narrowly defined age group or identified sensitive subpopulation. To account for such variability in the development of PRGs, which implicitly incorporate all exposure assumptions, the USEPA uses upper-bound parameter values. The effect of incorporating multiple upper-bound values into the PRG calculation results in a substantial overestimation of the reasonable maximum exposure. On the basis of the information discussed above, the net overall uncertainty associated with assessing exposure is moderate to high with a bias toward overestimation of risk.

Uncertainties in this PRE are also related to the use of USEPA-derived toxicity values. For chemical risk drivers, animal data served as the principal basis of the toxicity values used to develop PRGs. Extrapolation from animals exposed to high doses to humans potentially exposed to much lower doses is a major source of uncertainty influencing chemical toxicity and, consequently, the evaluation of risks. Furthermore, the use of uncertainty factors, typically ranging from 100 to 1,000, in the derivation of USEPA reference doses introduces additional uncertainty, biased toward overstating the actual toxic potential. Similarly, the use of the UCL 95 on the slope of the linear dose-response curve for carcinogens introduces additional uncertainty, biased toward overstating the

actual toxic potential. On the basis of the information discussed above, the net overall uncertainty associated with the toxicity values is moderate to high with a bias toward overestimation of risk.

The summation of RME risks across pathways is also conservative. According to the USEPA (1989), multiple-pathway RME risks could be best presented by a combination of a single-pathway RME and other average risks. As a result of compounding conservatism, the actual risks, if any, are likely to be less than the RME estimates presented in this PRE (USEPA 1989).

Based on this evaluation of uncertainty, it can be concluded that the overall uncertainty associated with the risk estimates presented in this PRE are moderate to high with a bias toward overstating actual risks.

### 5.2.3 PRE CONCLUSIONS AND RECOMMENDATIONS

Exceedances in USEPA Region 9 Industrial Soil PRGs were observed for several chemicals found at the Area 41 and Area D sites. Although exceeding industrial screening risk criteria, under industrial use scenarios, screening RME carcinogenic risks for both Area 41 and Area D site soils were within USEPA regulatory levels of concern (1E-04 to 1E-06). Carcinogenic risk drivers for Area 41 were Dieldrin, 4,4'-DDD, 4,4'-DDT, gamma-Chlordane, and Benzo(a)pyrene. Carcinogenic risk drivers for Area D were arsenic, 4,4'-DDT, and Trichloroethene. Dioxin concentrations found at the site were below regulatory risk criteria. The maximum dioxin/furan TEQ concentrations detected in Area 41 and Area D were 2.34 parts per trillion (ppt) and 1.05 ppt, respectively. The industrial soil PRG for 2,3,7,8 TCDD is 16 ppt. The USEPA OSWER directive cleanup level goal for dioxin and related compounds is 5-20 ppb TEQ.

Screening RME noncarcinogenic risks for site soils do not exceed USEPA's upper bound risk level of 1.0. The maximum concentration of lead in surface and subsurface soils was also below the screening risk values. Noncancer health effects are not expected to occur from exposures assumed in this preliminary risk assessment.

Groundwater at the Area 41 and Area D sites are not drinking water sources. Consequently, a comparison of groundwater concentrations to USFK EGS drinking water standards is not appropriate. The drinking water exposure pathway is incomplete. This

PRE makes such a comparison only to confirm that groundwater at the site not be used for drinking water. The data indicates that exceedances in groundwater were limited to VOCs and pesticides. As reported above, previous groundwater investigations report relatively widespread contamination of the aquifer throughout the base.

Based on the results of this PRE, the following conclusions can be made:

- Estimated potential carcinogenic risks associated with current and future industrial exposures to site soils are within USEPA's target risk range (1E-6 to 1E-4).
- Under current and future industrial site use scenarios, hazard indices associated with receptor exposure to site soils are below 1, indicating that there is little potential for noncarcinogenic health effects to occur given current site conditions.
- Although exceedances in EGS drinking water standards were observed, comparison of these standards to the data collected at the site is inappropriate. Groundwater at the Area 41 and Area D sites are not drinking water aquifers. The ingestion pathway is incomplete. Furthermore, previous groundwater investigations report relatively widespread contamination of the aquifer throughout the base. Background chemical contributions are probable.
- No remedial actions are recommended at this time.

## **SECTION 6**

### **REMEDIAL ALTERNATIVES EVALUATION**

---

The sections above show that the material disposed of in Area D has impacted both soils and groundwater to some extent. The soils contain several compounds that were detected at concentrations less than the health risk guidelines evaluated in the PRE. Groundwater in the vicinity of Area D contains dioxins, VOCs, and other compounds. Some groundwater contaminant concentrations exceed the respective EGS values, however, because the water table aquifer is not used for drinking water purposes, the EGS values are overly conservative and not applicable as cleanup standards under anticipated site usage. On the basis of the PRE results, no remedial actions are currently recommended at the site. However, recommended additional site characterization may reveal contaminant concentrations that exceed risk guidelines. This section evaluates potential remedial alternative actions that may be applicable in the future.

Groundwater contamination is understood to be a site-wide issue. The evaluation of remedial alternatives to treat groundwater directly is beyond the scope of this report. Rather, the remedial alternatives selected for evaluation were reviewed for their ability to reduce potential human health risk caused by exposure to contaminated soil, and for their ability to reduce continuing impacts to groundwater from the contaminated soil.

Four remedial alternatives were evaluated. The four alternatives include:

- 1) no remedial action;
- 2) capping with a geosynthetic liner;
- 3) capping without a geosynthetic liner; and,
- 4) removal of contaminated material.

These actions are discussed in more detail below.

It should be noted that the full extent of contaminants in the soil in Area D is not known. In particular, clean samples were not obtained to the north-west and south-west; and the area to the north-east is also not fully defined. We have made reasonable assumptions on

the extent of impacts beyond the samples taken; but additional delineation is recommended.

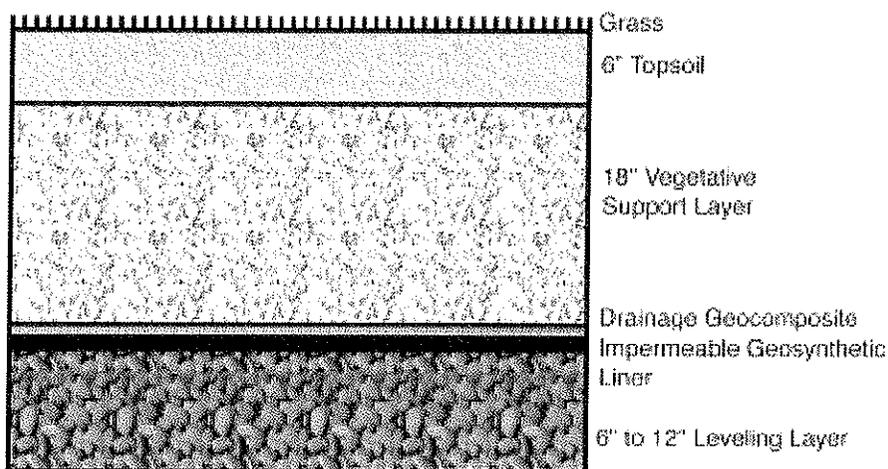
### 6.1 NO REMEDIAL ACTION

For this action, nothing is done to the site. There is no capital cost and no operations and maintenance cost. Precipitation will continue to leach contaminants from the soil into the underlying groundwater. Unprotected site workers will continue to be exposed to impacted soils. To prevent exposure to site contaminants, site access would need to be restricted to workers wearing appropriate personal protective equipment (PPE).

### 6.2 CAP WITH A GEOSYNTHETIC LINER

For this option, the site will be contoured to direct run-off away from the impacted area by adding clean fill material. A geosynthetic cap, meeting RCRA Title 35 Subtitle C criteria, will be constructed over the impacted site. This cap will likely consist of a 6 to 12 inch thick leveling and bedding layer; an impermeable geosynthetic liner, a drainage geocomposite, an 18" thick vegetative support layer and a 6" layer of topsoil. Grass will be established in the topsoil layer.

Cap with Geosynthetic Liner



Operations and maintenance (O&M) will consist of mowing the grass, preventing intrusive work in the area, and occasional repairs to the topsoil layer to maintain surface contours. Groundwater monitoring should also be performed regularly.

This option will provide a boundary to prevent human contact with the contaminated soils. No precipitation infiltration will occur; therefore, there will be no leaching of contaminants to groundwater.

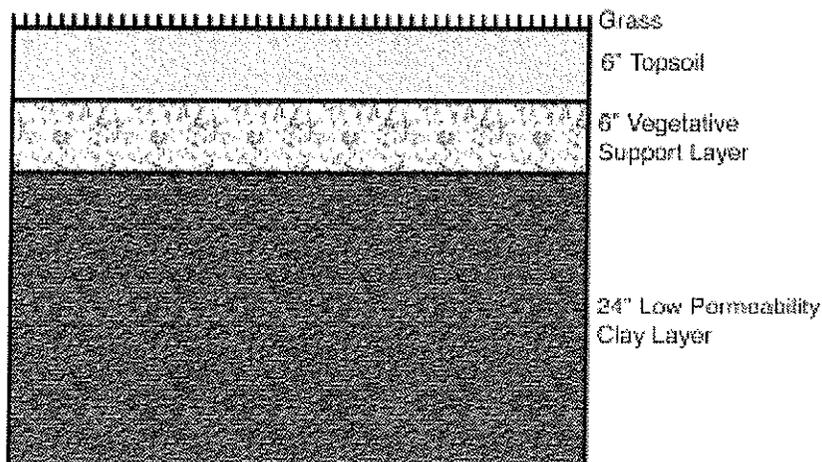
Construction is relatively straightforward, and poses little additional risk to workers. Capital costs are estimated at \$179,000, and O&M costs are estimated at \$2,650 per year.

### **6.3 CAP WITH A CLAY LINER**

This option is similar to Option 2 above, except that a clay liner is substituted for the geosynthetic liner, and the cap is not designed to meet RCRA Title 35 Subtitle C criteria. The site will be contoured to direct run-off away from the impacted area by adding clean fill material. A clay cap will be constructed over the impacted site. This cap is assumed to consist of a 24" thick low-permeability clay layer, a 6" thick vegetative support layer, and a 6" layer of topsoil. Grass will be established in the topsoil layer.

Operations and maintenance will consist of mowing the grass, preventing intrusive work in the area, and occasional repairs to the topsoil layer to maintain surface contours. Groundwater monitoring should also be performed regularly.

### Cap with Clay Liner



This option will provide a boundary to minimize human contact with the contaminated soils. Precipitation infiltration will be greatly reduced (but not completely stopped); therefore, there will be only minimal leaching of contaminants to groundwater.

Construction is relatively straightforward, and poses little additional risk to workers. Capital costs are estimated at \$105,000, and O&M costs are estimated at \$2,900 per year.

#### 6.4 REMOVAL OF CONTAMINATED SOILS

For this option, the dioxin-impacted soils in Area D will be excavated and hauled off site for treatment and/or disposal. It is estimated that approximately 57,950 cubic yards will be excavated for offsite disposal and treatment (see Figure 6-1). It is assumed that excavated materials will be disposed of by shipment to the United States followed by thermal treatment (due to the presence of dioxins). Following excavation, clean fill will be placed back into the excavation and contoured. Once the excavation is complete, no O&M is required.

This option will eliminate the potential for human contact with the contaminated soils. There will be no leaching of contamination to groundwater, since all soil contamination will be removed.

The execution of the remedial action is relatively complicated, with significant handling of contaminated materials. There is an increased risk of exposure to workers during excavation and trucking. Capital costs are estimated at \$93,800,000, and no O&M costs are anticipated.

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## **SECTION 7**

### **CONCLUSIONS AND RECOMMENDATIONS**

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Conclusions and recommendations for the SI conducted at Area 41 and Area D of Camp Carroll are presented in the following sections.

#### **7.1 CONCLUSIONS**

This SI was initiated to investigate possible soil and groundwater contamination associated with a former hazardous waste drum storage area (Area 41) and a temporary landfill (Area D). The SI was designed to evaluate the nature and extent of existing contamination, to determine groundwater flow patterns and potential contaminant migration pathways, and to evaluate several potential remedial alternatives.

The SI included the following field activities: Site reconnaissance; geophysical survey, exploratory trenching, exploratory drilling; installation monitoring wells; soil and ground-water sampling; water level monitoring in wells; and aquifer testing. Soil and groundwater samples were analyzed at offsite analytical laboratories.

The following conclusions concerning the site have been developed based on the data acquired during the SI:

#### **Geology and Hydrology**

- The site is underlain by granitic bedrock which is covered by varying thicknesses of weathered granitic bedrock material (saprolite) and fill soils derived from a similar source rock. Fractures and faulting were not observed in soil cores during the drilling activities.
- The measured groundwater level within the monitoring wells at Area 41 is approximately 13 feet to 33 feet (4 to 10 meters) bgs, at elevations of approximately 95 feet to 115 feet (29 to 35 meters) msl. The measured groundwater level within the monitoring wells at Area D is approximately 23 feet to 33 feet (7 to 10 meters) bgs, at elevations of approximately 131 feet to 141 feet (40 to 43 meters) msl. The groundwater gradient at each of

the two areas investigated is directed to the west. If additional groundwater level information becomes available from other locations within or in the vicinity of the site, the interpreted groundwater flow patterns may require modification.

- On the basis of the available site data, groundwater and aqueous phase contaminants will tend to flow toward the west with the groundwater gradient when the subsurface lithology is permeable in that direction. On the basis of groundwater contaminants measured in existing monitoring wells located to the west of Area 41 and Area D, a preferred westward migration pathway is consistent with the observed data at each Site.

#### Assessment of Soil and Groundwater Impacts

- On the basis of a geophysical survey and exploratory trenching conducted at Area D, it is considered likely that buried drums containing hazardous materials at the site have previously been excavated and removed.
- Soil samples obtained from Area 41 contained concentrations of numerous contaminants including TPH-G, TPH-D, TPH-O, VOCs, SVOCs, pesticides, RCRA metals, and dioxins. Several soil contaminant concentrations exceeded PRG screening criteria, however, contaminant concentrations are less than the risk criteria evaluated in the PRE. Groundwater samples obtained from Area 41 monitoring wells contained concentrations of TPH-G and TPH-D, VOCs, RCRA Metals, and dioxins. Detected concentrations that exceeded EGS values for groundwater are limited to VOCs. EGS values are not considered appropriate cleanup criteria for the site because the water table aquifer is not used for drinking water purposes in the area.
- Soil samples obtained from Area D contained concentrations of numerous contaminants including TPH-G, TPH-D, TPH-O, VOCs, SVOCs, pesticides, RCRA metals, and dioxins. Several soil contaminant concentrations exceeded PRG screening criteria, however, contaminant concentrations are less than the risk criteria evaluated in the PRE. Groundwater samples obtained from Area D monitoring wells contained

concentrations of TPH-G and TPH-D, VOCs, SVOCs, pesticides, RCRA Metals, and dioxins. Detected concentrations that exceeded EGS values for groundwater are limited to VOCs and pesticides. EGS values are not considered appropriate cleanup criteria for the site because the water table aquifer is not used for drinking water purposes in the area.

- Contaminants identified in existing groundwater monitoring wells located to the west of Area 41 and Area D are consistent with a westward direction of groundwater flow and migration of aqueous contaminants at each of these areas. However, a baseline groundwater investigation conducted by Woodward Clyde Consultants (WWC 1992b) reported relatively widespread chlorinated solvent contamination of the aquifer throughout the base. The detection of VOCs in wells located hydraulically upgradient of each site investigated may indicate elevated background concentrations of these compounds in the area.
- Despite potential elevated background VOC levels, several groundwater samples contained relatively high concentrations of chlorinated solvents that suggest a local source. In particular, sample CC054WS01 obtained from monitoring well M03-470 in Area 41 contained a reported tetrachloroethene concentration of 11.1 mg/L and sample CC237WS01 obtained in monitoring well M03-465 in Area D contained a reported trichloroethene concentration of 1.4 mg/L. Cis-1,2-dichloroethene concentrations were greater than 1.2 mg/L in monitoring well M03-465 (samples CC037WS01, CC137WS01, and CC237WS01). In addition, sample CC024WS01 contained the pesticide Lindane with a concentration of 8.76 mg/L.

#### Conceptual Site Model

- The subsurface environment appears to be comprised of weathered granitic bedrock and fill materials derived from similar source rock. No preferred fracture orientations were observed during drilling activities. The direction of groundwater flow and migration of aqueous contaminants are presumed to be consistent with the hydraulic gradient.

- The identified groundwater gradient at each of the two sites investigated is directed toward the west. It appears that aqueous phase contaminants originating in shallow soils may have migrated downward through the vadose zone to the groundwater table, and then laterally towards the west with groundwater flow. The observed presence of similar contaminants in groundwater wells located to the west of Area 41 (Monitoring Well MW-14) and Area D (Monitoring Well MW-23) are consistent with this scenario.

## 7.2 RECOMMENDATIONS

On the basis of the information and analytical data obtained during the site investigations performed in Area 41 and Area D, the recommendations to address COPCs at Camp Carroll include:

- Additional groundwater investigation is recommended at both Area 41 and Area D to further evaluate the observed concentrations of chlorinated solvents. A 1992 baseline groundwater investigation of the Site (WWC 1992b) reported relatively widespread contamination of the aquifer throughout the base.
- Additional soil investigation is recommended at Area D to further define the limits of impacted soil and the boundaries of the former landfill.
- No remedial actions are recommended at this time. In the event that additional site characterization indicates that contaminant concentrations exceed risk criteria in Area D, it is anticipated that capping of the landfill area using a clay cap will be the preferred method to provide a barrier to human contact with impacted soils and to limit infiltration through the impacted soils.

**SECTION 8**  
**REFERENCES**

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- OEES. 1999. Standard Operating Procedures Manual.
- Samsung, 2002a. *Sampling and Analysis Plan for Camp Carroll Area D and Area 41 Site Investigations, Camp Carroll, Korea.*
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- Woodward-Clyde Consultants (WWC), 1992a. *Historical Land Use and Background Survey Report, Camp Carroll, Korea. June 1992.*
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## **Appendix A**

### Geophysical Survey Results

Final Report

Geophysical assessment to a landfill site in  
Camp Carroll, Waegwan, Korea

May 2003

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**Geophysical assessment to a landfill site in Camp Carroll,  
Waegwan, Korea**

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Figure 5. Schematic diagram for typical HLEM survey. The survey can be either the horizontal coplanar (HCP) or the vertical coplanar (VCP) configuration.

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## 1. Introduction

Area D (Figure 1) in Camp Carroll has been identified as a former hazardous waste landfill. Numerous hazardous materials were disposed in this landfill between the years of 1977 and 1982. Personnel interviews indicated that many drummed hazardous materials were transported from Area 41. The landfill dimensions were approximately 500 feet by 250 feet in area; and 20 to 30 feet deep (Figure 2). Reportedly, much of the filled materials and surrounding soil was excavated between 1982 and 1983 and placed into 55-gallon drums. Despite the removal activity, residual amounts of contaminated material may have remained.

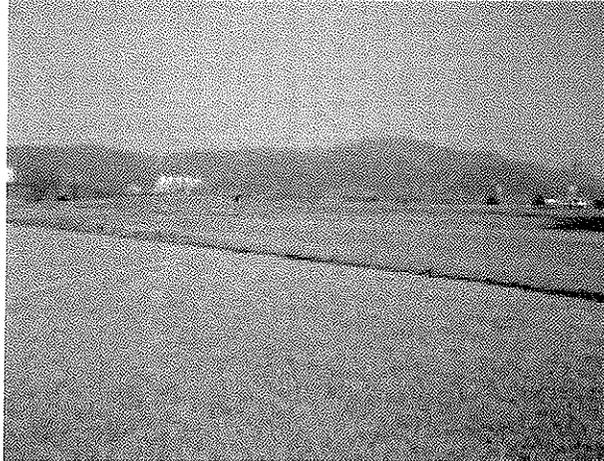


Figure 1. An overview of Area D in Camp Carroll

In this project, two different geophysical approaches have been made to characterize the landfill site. The objectives of geophysical survey can be summarized by following two; 1) defining the thickness of the landfill or the depth to the bedrock, and 2) locating the buried metallic objects such as drums, if they still remains. Two different approaches have been made for each objective; DC resistivity method for the former, and horizontal loop electromagnetic (HLEM) method for the latter.

Electrical properties of a medium are mainly dependent on the ion contents of pore fluid as well as clay contents of the soil (Keller, 1988). Typical waste disposal site shows three-layered structure; the landfill on top, residual soil on the middle, and the bedrock on the bottom. Usually the resistivity of the landfill and the residual soil is smaller to the bedrock. Residual soil shows lowest resistivity among them. Residual soils commonly contain much of clay rather than sand. The

landfill, however, commonly contains plenty of sand other than clay, which makes its resistivity larger than that of the residual soils underneath the landfill. DC resistivity method shows very strong features to map the layered earth model (Dobrin, 1976).

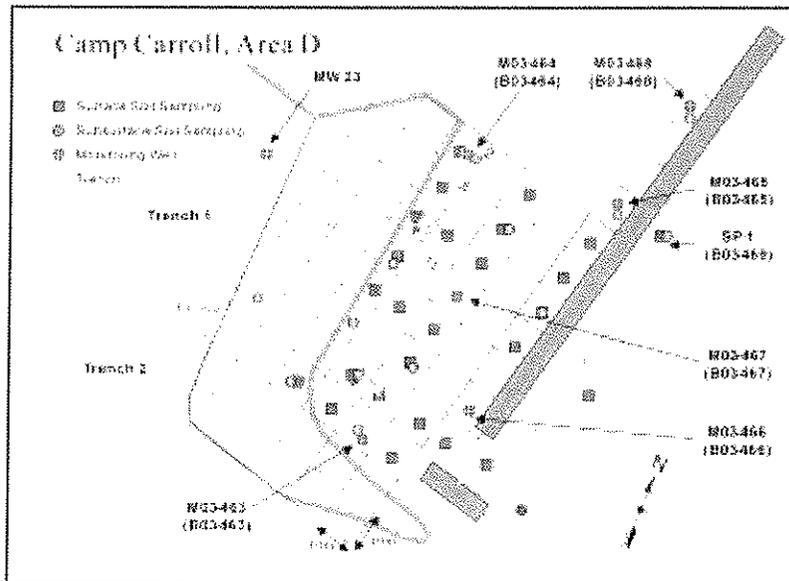


Figure 2. Site map of Camp Carroll landfill area

Electromagnetic (EM) survey, horizontal loop EM (HLEM), can give us an useful information about the location of the metallic objects, if they are within the landfill. The depth of investigation of HLEM ranges up to 20 m depending on the frequency it uses and the conductivity of the medium (Song et al., 2001).

By integrating the two methods in this project, geo-electrical structures for the landfill site as well as the position of potential buried metallic objects (e.g., drums or other containers) can be identified.

## 2. Theories & Methods

### 2.1 Horizontal Loop Electro-Magnetic method (HLEM)

HLEM transmits HF band (kHz ~ tens of kHz) electromagnetic waves. The transmitted primary electromagnetic (EM) fields induce the eddy currents in the metallic (conductive) objects beneath the earth. The eddy currents, in turn, make secondary EM fields as shown in figure 3. Measuring the secondary field with small loops on the surface, one can figure out the location of the anomalous body as well as the conductivity of the ground.

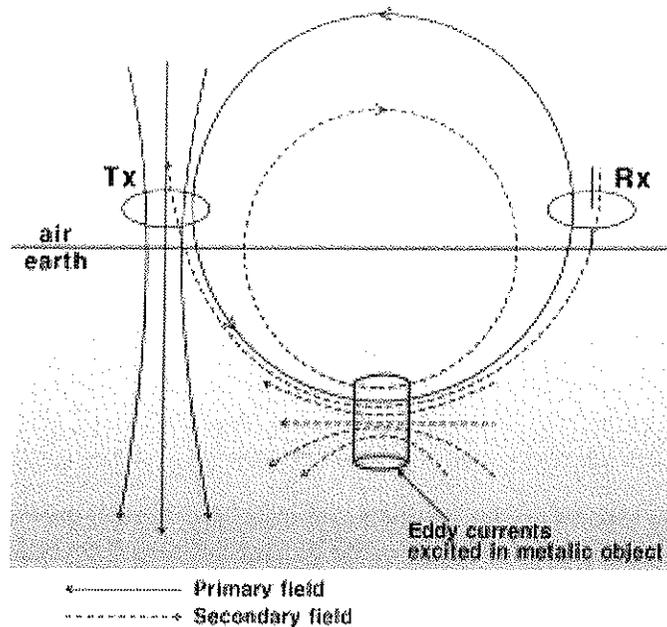


Figure 3. Theory of horizontal loop electromagnetic (HLEM) method.

Figure 4 and Figure 5 shows typical HLEM survey procedure and typical responses of buried metallic sphere, respectively. EM31 provides two types of measurements; i.e., horizontal coplanar (HCP) and vertical coplanar (VCP) arrays. Apparent conductivity can be calculated from both modes but HCP configuration is a little more sensitive to the buried targets than VCP configuration (Frischknecht et al., 1991). Note that the minimum or maximum peaks at the right position of the buried objects.

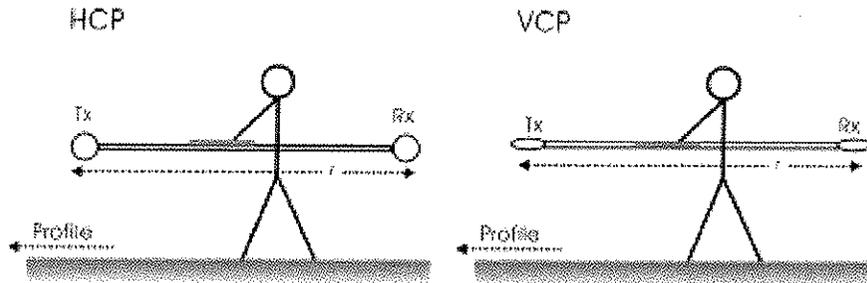


Figure 4. Schematic diagram for typical HLEM survey. The survey can be either the horizontal co-planar (HCP) or the vertical co-planar (VCP) configuration.

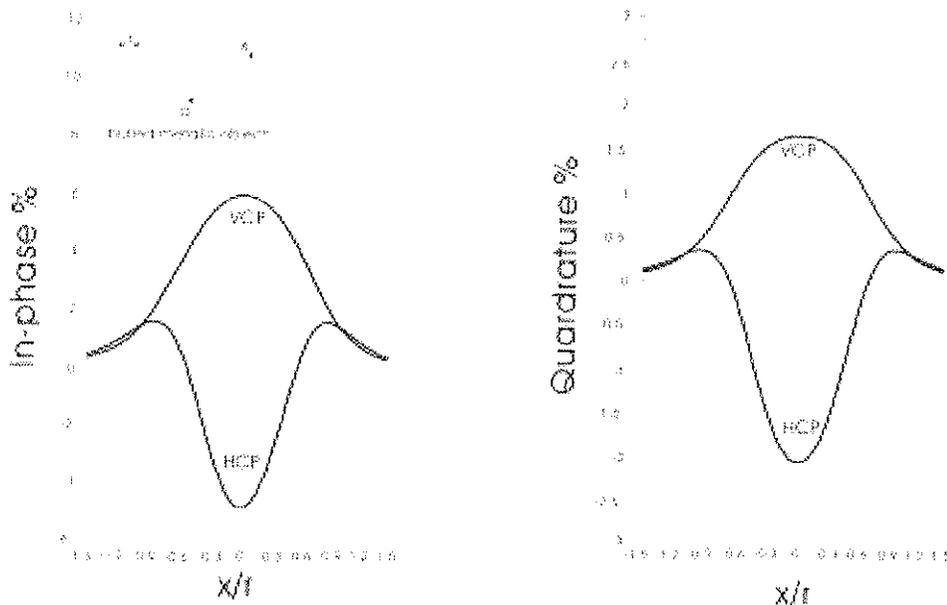


Figure 5. Schematic diagram for typical HLEM survey. The survey can be either the horizontal coplanar (HCP) or the vertical coplanar (VCP) configuration.

Apparent resistivity ( $\rho_a$ ) can be calculated from both configurations by

$$\frac{1}{\rho_a} \approx \frac{4}{\mu_0 \omega r^2} \times (\text{Quadrature reading}) \quad (1)$$

where,  $\omega$  is angular frequency,  $\mu_0$  is magnetic permeability in free space, and  $r$  is the distance between the transmitter and the receiver.

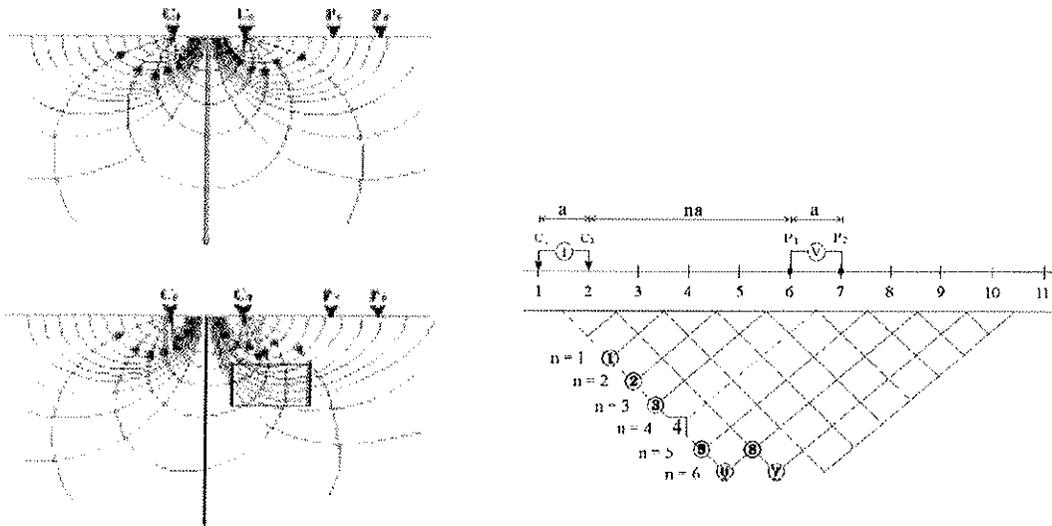
## 2.2 DC resistivity (dipole-dipole) survey

Dipole-dipole survey needs two current electrodes and two potential electrodes. The potential induced by transmitted current is disturbed by underground inhomogeneities (Figure 6). Dipole-dipole survey measures the potential distribution on the surface with fixed current/potential electrode spacing. The bigger the separation between the current electrodes and the potential electrodes is, the deeper information the data carries. With moving the potential electrodes with fixed separation, normalized potential with applied current ( $\Delta V / I$ ) is measured (Figure 7). The measured data is converted to apparent resistivity by multiplying the geometric factor ( $G$ ):

$$\rho_a = G \frac{\Delta V}{I} \quad (2)$$

$$G = -2\pi(n-1)n(n+1)a$$

The geometric factor is dependant on the electrode spacing ( $a$ ) and the spread number ( $n$ ) illustrated in Figure 7. Two-dimensional resistivity image can be gathered by inversion process using the apparent resistivity. A commercial software Dipro4Win was used for inversion of the data.



Stacking will improve signal to noise (S/N) ratio. Maximizing transmitting power (current) is another good way of improving S/N ratio. ABEM Terrameter (model SAS300C) provides 2mA to 500mA transmitting currents selectable depending on the resistivity of the earth. In most of cases, 20mA of currents were transmitted in this survey.

850

### 3. Geophysical survey design

Twelve HLEM survey lines were set up to form two-dimensional grid on the surface as shown in Figure 8. The main purpose of the HLEM survey is to detect any metallic objects (drums) beneath the earth. When plotting 2-dimensional contours of the resistivity measured, closed contours will be concentrated on the right place where a metallic objects is buried.

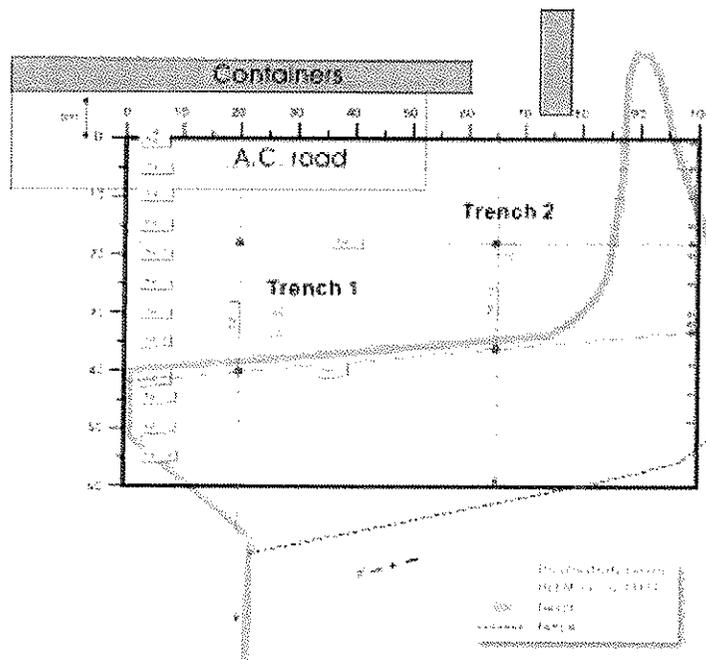


Figure 8. Survey lines for HLEM (blue) and DC resistivity method (red)

At every survey line, the HLEM data have been collected at every 2m for both vertical co-planer (VCP) and horizontal co-planer (HCP) configuration of the source and receiver coils. Though, in-line configuration of the coils (the TX coil and RX coils are in-line with the survey lines) was used to minimize the interferences by the containers and by the fences around the survey area, they will inevitably affect the data near to them.

Four DC resistivity survey lines are set up to find out the depth to the residual soils and/or bedrock; two of them are in N-S directions and the other two are perpendicular to them (red lines in Figure 8). The dipole spacing for Line-1 and Line-2 are set to 5m, and for Line-3 and Line 4 to 3m, of which maximum penetration depth is 25m and 15m, respectively.

## 4. Results and Interpretations

### 4.1 DC resistivity (dipole-dipole) survey

Figure 9 shows the inversion results of the four DC resistivity surveys. Generally speaking, the resistivity sections show the characteristics of the two-layered earth. The top layer shows high resistivity and the bottom shows relatively low resistivity for all the four sections. The top layer with high resistivity (ranged from 100 ~500 ohm-m) can be the landfill material over the groundwater level, while the bottom layer with lower resistivity (below 100 ohm-m) can be the residual soil below the groundwater level. They say that the area used to be an agricultural field before the landfill. The residual soil in agricultural fields shows the characteristics of fine-grained, low permeability, high water contents, and thus low resistivity. Estimated boundary between the landfill materials and the residual soils are overlain in each resistivity sections. The boundary shows almost flat except for Line-3 and the thickness of the landfill ranges 3 to 7 m.

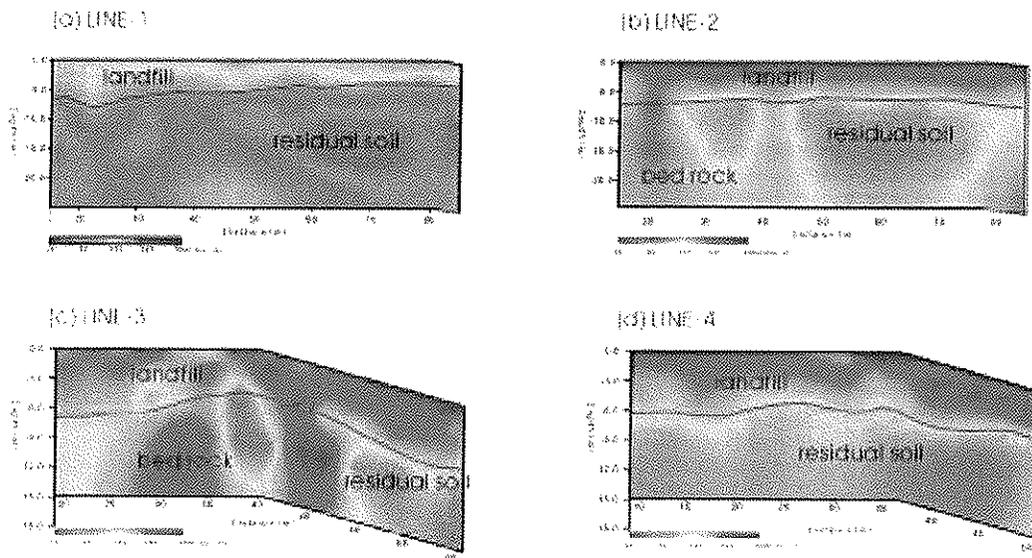


Figure 9. Resistivity sections from DC resistivity survey for the four lines shown in figure 8.

High resistivity below 10m (a few hundred ohm-m) can be the bedrock underneath the residual soils. Note that it appears only at the left side in Line-2 and at the center of Line-3. One cannot find such layer from Line-1 and Line-4. The bedrock can lie deeper than 20 m in Line-1 and Line-4.

The resistivity of groundwater normally shows from about 50 ohm-m to a few hundreds ohm-m depending on its mineral contents. The more the groundwater contains the metallic mineral, the smaller the resistivity of the groundwater. From the extra-ordinarily low resistivity of the second layer (especially at around 70m in Line-1), which shows 30 ~80 ohm-m, we have a doubt that the groundwater may contains various kind of metallic mineral or be contaminated.

Figure 10 shows a 3-D view of the DC resistivity results. Note that high resistivity zone of 3<sup>rd</sup> layer is concentrated to the NW part of the site. We assumed that this high resistivity zone indicates the bedrock. The bedrock is seated deeper than 20 m in SE part, while at around 10m in NW part of the survey area (marked A in the figure).

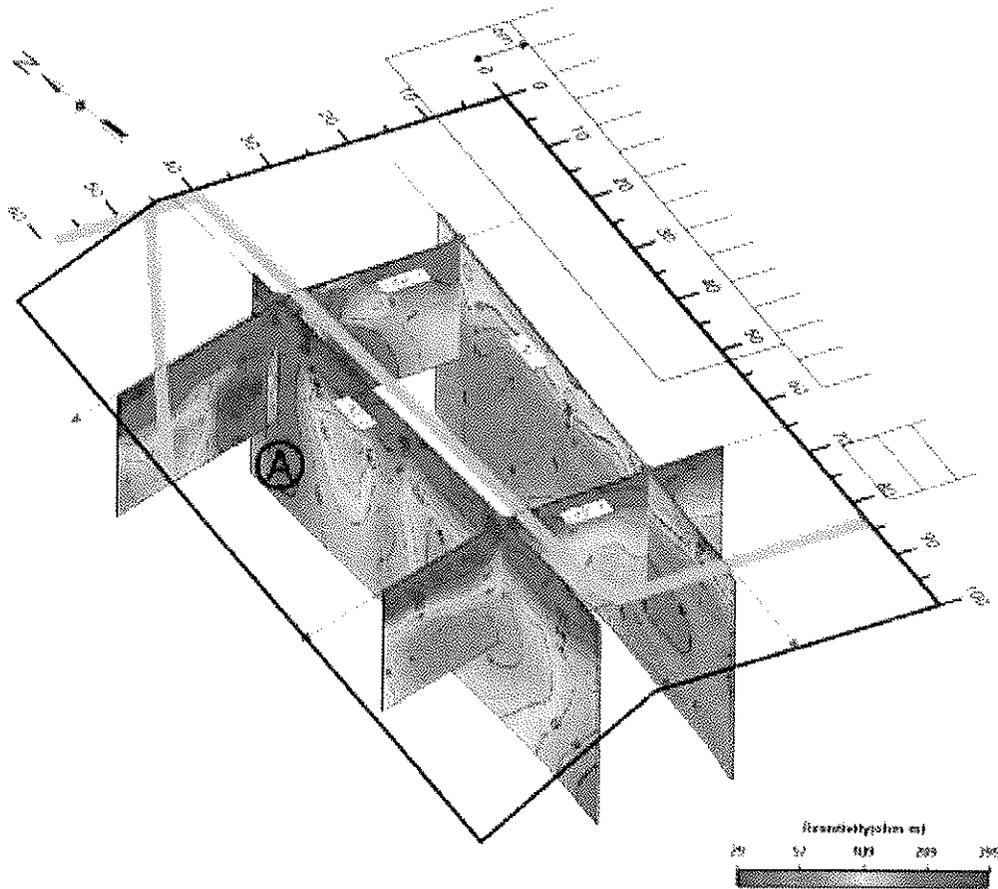


Figure 10. 3-D view of electrical resistivity distribution from DC resistivity survey

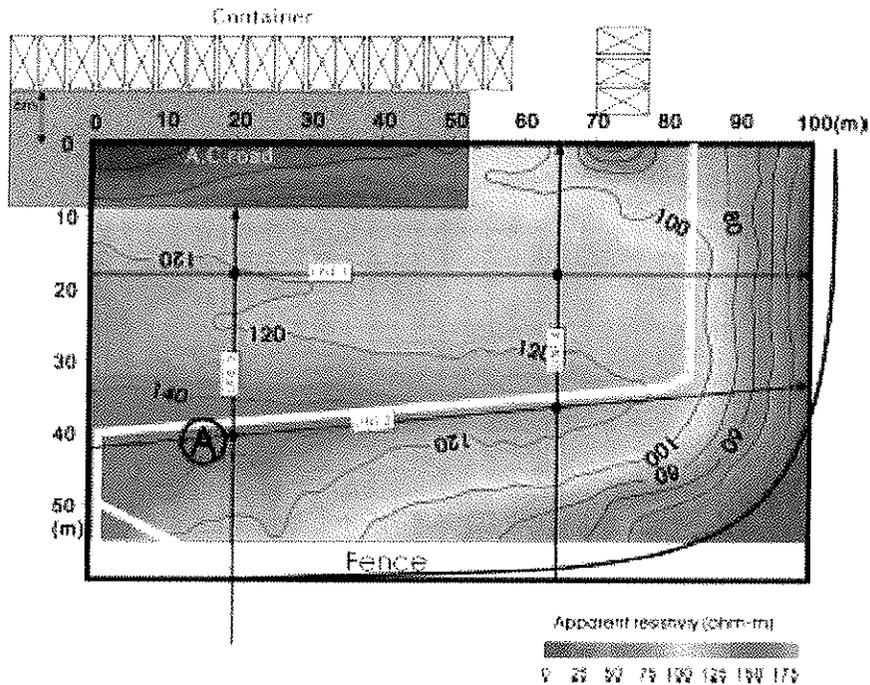
853

#### 4.2 HLEM survey

Figure 11 shows the apparent resistivity contours from the HLEM survey. Apparent resistivity contours from VCP and HCP shows very similar results, except for the resistivity values. VCP shows slightly high apparent resistivity values than HCP.

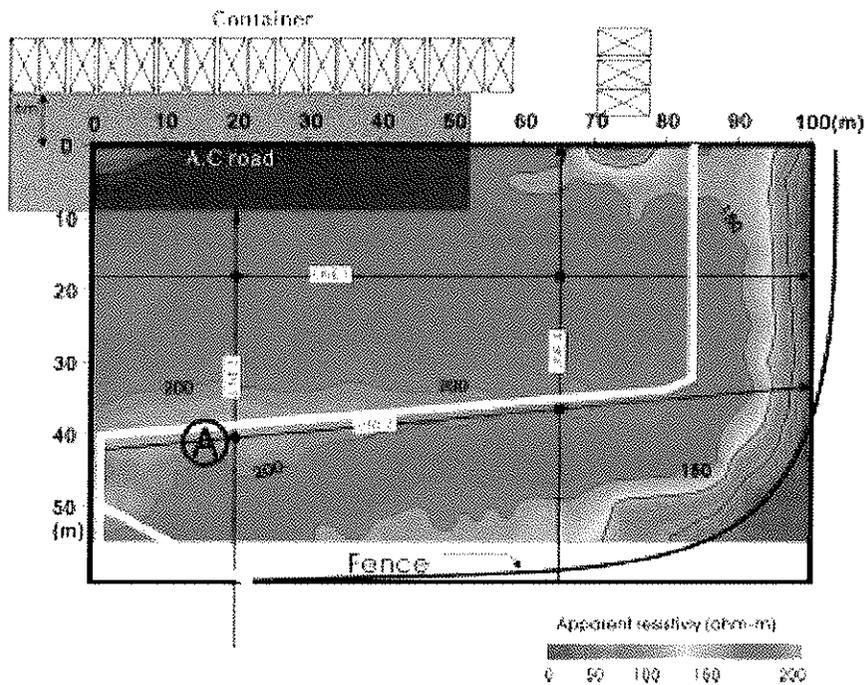
The HLEM methods are very sensitive to the nearby metallic objects. Note that the fences and the containers affect the HLEM data and appear as low resistivity anomalies (below 100 ohm-m) surrounding the survey area. Excluding them, any conductive anomaly couldn't be found within the region. This, in turn, implies us that no more metallic drums are exists within the survey area. Overall apparent resistivity of the ground lies at around 100 ohm-m.

Note the high resistivity anomaly at the marking point (A). This high resistivity anomaly is consistent with the high resistivity zone in DC resistivity survey above. As mentioned in DC resistivity section, the bedrock seems to lie in shallow depth (about 10 m) at the marking point A. Shallow bedrock will affect the HLEM data and appears as high resistivity anomaly.



(a) HCP

854



(b) VCP

Figure 11. Apparent resistivity contours from HLEM survey

### 4.3 Integrated interpretations

Backhoe excavation has been carried out on two spots indicated in Figure 2. Figure 12 shows the resistivity sections from two different geophysical methods, HLEM and DC resistivity, with the pictures after the excavation. As expected in Trench 1, the residual soil came out at the depth of about 4~ 4.5 m from the surface, which is right depth where it shows low resistivity anomaly in resistivity section of Line-3 as indicated in the figure. The upper part of the residual soil (the landfill) showed almost homogeneous sand layer, which forms the high resistivity top layers in resistivity sections. Residual soils, however, has not been found in Trench 2 through about 5m from the surface. As can be seen from the resistivity section from Line-4, the boundary to the residual soil layer lies in around 6m in depth, which is somewhat deeper than at Trench 1.

Any drums or metallic objects could not be found, which, in turn, shows us why any conductive anomaly did not appear in HLEM data.

855

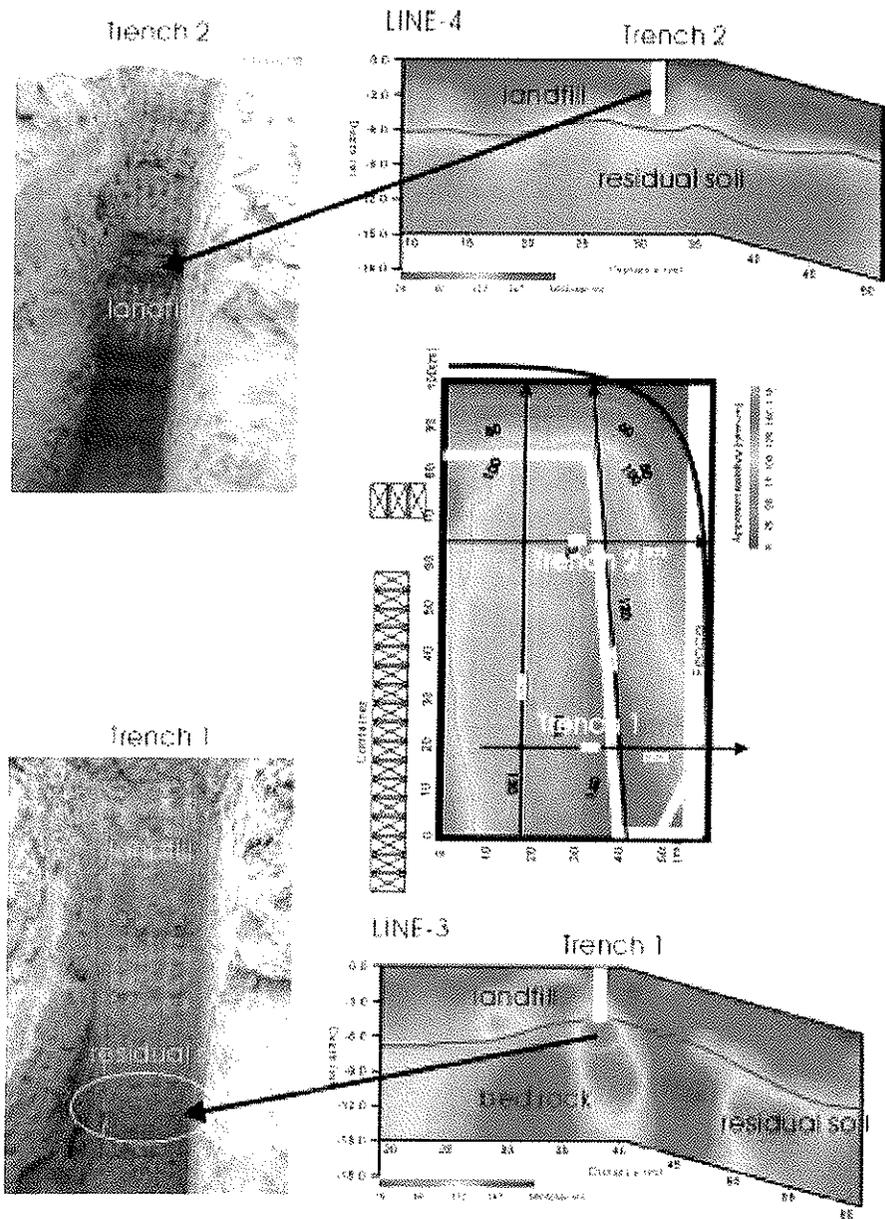


Figure 12. Integrated interpretation of geophysical methods (HLEM and DC resistivity) with backhoe excavation.

## 5. Conclusions and remarks

Horizontal loop electromagnetic method (HLEM) and DC resistivity survey has been carried out to characterize the landfill and potential buried drums or metallic objects. Both of the geophysical data showed very consistent results with each other. The resistivity of the landfill ranges from 100 ~ 250 ohm-m, while that of residual soils is a few tens of ohm-m. The bedrock in this area seems to reach deeper than 20m in most parts of the area. An exception is NW part, where the bedrock depth seems to be within 10 m.

Two-dimensional resistivity section clearly showed the boundary between the landfill and the residual soils. The boundary lies between 3 to 6 m in depth. Backhoe excavation also confirmed it. No conductive anomaly by any buried metallic objects was found in 2-dimensional apparent resistivity contour map from HLEM survey. Ground resistivity showed homogeneous feature all through the area.

Though we couldn't find any proof that metallic drums are still remains within the landfill, careful attention should be paid to the extra-ordinal low resistivity anomaly (below 50 ohm-m) in the resistivity section from DC resistivity survey, see 70m from left in Line-2 section in Figure 9. This can be either some kind of conductive objects including metallic drums or the groundwater contaminated by various ionic solutions as well as heavy metallic ions. The latter is more consistent with *a-priori* information of the site as well as geophysical interpretation in following two reasons;

- 1) The anomaly doesn't appear within the landfill layer, but in depth over 15m below the residual soils. There is no reason that metallic drums are buried within the residual soil layer.
- 2) The anomaly only appears in DC resistivity. The HLEM method, which is more sensitive to the concentrated metallic objects than DC resistivity, couldn't show the anomaly. In HLEM data, the resistivity in that part shows slightly lower than other parts instead. This suggests us that the anomaly is not any concentrated body but spread widely.

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## **Appendix B**

Field Logbook and Notes

859

MEASUREMENT CONVERSIONS

IF YOU KNOW MULTIPLY BY TO FIND

LENGTH		
inches	2.540	centimeters
feet	30.480	centimeters
yards	0.914	meters
miles	1.609	kilometers
millimeters	0.039	inches
centimeters	0.393	inches
meters	3.280	feet
kilometers	1.093	yards
	0.621	miles

WEIGHT		
ounces	28.350	grams
pounds	0.453	kilograms
grams	0.035	ounces
kilograms	2.204	pounds

VOLUME		
fluid ounces	29.573	milliliters
pints	0.473	liters
quarts	0.943	liters
gallons (U.S.)	3.785	liters
milliliters	0.033	fluid ounces
liters	1.055	quarts
liters	0.264	gallons (U.S.)

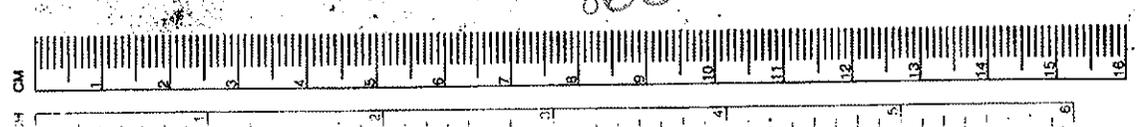
TEMPERATURE		
$^{\circ}\text{C} = (\text{F} - 32) \times .555$		
$^{\circ}\text{F} = (\text{C} \times 1.8) + 32$		

Inches	Decimals	Mil:
1/16	.0625	1.5875
1/8	.1250	3.1750
3/16	.1875	4.7625
1/4	.2500	6.3500
5/16	.3125	7.9375

3/8	.3750	9.5250
1/2	.5000	12.7000
5/8	.6250	15.8750
3/4	.7500	19.0500
7/8	.8750	22.2250

1"	1.0000	25.4000
2"	2.0000	50.8000
3"	3.0000	76.2000
4"	4.0000	101.6000
5"	5.0000	127.0000

6"	6.0000	152.4000
7"	7.0000	177.8000
8"	8.0000	203.2000
9"	9.0000	228.6000
10"	10.0000	254.0000
11"	11.0000	279.4000
1 foot	1.0000	304.8000



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Howell, AZ 96817  
 Phone (808) 545-2462  
 Project Camp Carroll, KAREA  
Area D and Area 41

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①

Camp Carroll, Korea

4/10/03

ONBik 8:00 AM: AREA D

ARCC = [REDACTED] (PS)

Samsung: Principal in way to be = DMLee

Field MR = Yun, Jun, Ki.

My young head Nash = @/ac

+ Sandy soil field techniques & drills  
SEC (Beaumont) (number number) = drills

In soil borings (FED for wells)

Preparing for surface soil sampling

Selected grid locations to sample

will collect 27 surface samples

on regular grid with 10-meter

centers. Some locations limited

by site conditions (drainage

ditch, asphalt paving.) Surface

soil samples will actually be

collected beneath covered soils

to land fill, if this can be

decreased using a backhoe.

0915 excluded from marked

off. Each soil sampling grid

node has been assigned a location

number: 001 → 027. The

② 4/11/03 ③

SAME grid location numbers will be used for both surface soil samples and subsurface soil samples.

SAMPLE numbers will be assigned AS follows:

CC 001 SS 01

02 SS CC 02

where CC = CC for Camp Carroll  
SS = 001 - 027 for sample location ID  
CC = SS for surface soil or BS for boring  
01, 02, etc. for sample number (consecutive)

Subsurface soil boring & sampling will be conducted at 6 of these locations: tentatively at 006, 010, 017, 022, ~~026~~ 026, and 027.

Exploratory trenching will be conducted starting tomorrow to allow high geophysical and soil and of soil and subsurface conditions. 0920 began subsurface boring location 010 - direct push, split spoon sample. Cuts 1 = 0.3 - 0.5 m

Boring 1 - location 010  
0.3 - 0.5 m: Moist, strong brown  
7.5 YR 5/6, silty fine to coarse sand (SM), 100% recovery  
PID = 0.0 ppm, medium dense  
10:10 AM, some cobbles at 0.8 m

10:20: 0.9 m - 2.0 m: 80% Recovery  
SAME AS 0.3 - 0.5 m by thin clay & more cobbles (decomposing granitic quartzite). ~~some sand & gravel~~  
5 cm for gravel (5% G/80% 15% F) dense  
collected surface sample at 1.0 - 2.0 m  
CC 010 SS 01 (lowest fill cover)

Note: Surface soil sampling using bucket began at 10:30  
10:50: 1.0 m - 3.2 m, 80% Recovery  
2.0 - 2.6 m = same as above by 10:45.  
2.6 - 3.2 m = moist fine to medium sandy clay, 7.5 YR 5/6 strong brown with white to YR illite/montmorillonite  
11:20, low to medium plasticity (CL) some cobbles, increased moisture (some manganese oxide on faces at 2.1 m)  
(5% G/55% 60% F)  
[cut to medium dense = silty to fine sandy clay (CC)]

4

4/1/63

11:03 = 3.2m - 4.5m, 80% recovery  
 3.2m - 4.0m = moist, clayey to silty  
 fine to medium sand (SC-SM)  
 7.5% R 5/6 strong brown  
 (65% S / 35% F) dense  
 4.0 - 4.5m = moist, fine to medium  
 sandy clay, medium plasticity (CL)  
 (40% S / 60% F) 7.5% R 5/6  
 strong brown, firm  
 extra blocks - appears to be  
 siltstone - decomposed granitic,  
 quartz & feldspars, no cobbles.  
 11:30 = 4.7m - 5.8m, 95% recovery  
 4.7 - 5.2m = moist, clayey f-m sand  
 (65% S / 35% F) (SC) dense  
 7.5% R 5/6 strong brown  
 5.2 - 5.5 = moist, silty 4.7-5.2m but  
 silty gray 5% 4/2  
 5.5 - 5.8m = same but 7.5% R 9/8  
 strong brown, with some coarse  
 sands.  
 entire section appears to  
 be siltstone.  
 collected soil sample (CCD10B501a)

5

4/1/63

12:00 = 5.8m - 7.3m, 100% recovery  
 5.8 - 6.3m moist to 7.3m 5/4 yellowish  
 brown, clayey fine to med. sand,  
 dense. - good metal shavings, could  
 be sluff  
 6.3 - 6.8m = moist, unstratified, (65% S / 35% F)  
 clayey f-m sand (siltstone)  
 (SIL) color varies in bands &  
 patches from red 2.5% R 4/6  
 to silty brown 2.5% 4/4  
 - quartz & feldspar clasts, angular  
 6.8m - 7.3m = moist to wet f-m  
 sandy clay (CL) medium  
 plasticity, micaceous (35% S / 65% F), dark yellowish  
 brown to 7.3m 4/4  
 12:24 - 7.5m - 8.6m, 100% recovery  
 collect sample (CCD10B502)  
 moist to wet siltstone =  
 clayey f-m sand (SC) to f-m  
 sandy clay (CL) low to  
 medium plasticity, appears  
 (50% S 50% F)  
 12:30 Lund beach

(C)

4/1/63

1420 Begin drilling boring 2 at location 026

14:29: 1.0m - 2.5m 80% recovery moist, strong brown 7.5YR 5/6 clayey, f-fm sand (SC) with

some coarse sd. & fine gravel. (5.2 G/707-5/25% F) (dense), some cobble at 2.3m. PID=0.0ppm

14:40: 2.5m - 4.0m 90% recovery moist, strong brown 7.5YR 5/6

slightly to clayey f-fm sand. (USM - SKY). Apparent to

be weathered granitic (syenite) angular quartz & feldspar, mica.

PID = 0.0 ppm

15:00 4.0m - 5.5m, 80% recovery

4.0 - 5.0m = same as 2.5 - 4.0m

5.0 - 5.2m = moist clayey f-fm (SC) red 2.5YR 4/6

(0.57 J/357-F)

5.2 - 5.3m = 8.1% f-fm sd (SA)

with some trace clay, 1 yell-wish brown

10 YR 5/4

5.3 - 5.5m = clayey f-fm sd (SC)

(D)

4/1/63

[607.5/407. F]

follow with no 5YR 4/6

collect sample CC 006 B501

15:18: 5.5m - 9.6m 100% recovery

moist, clayey f-fm sd. (SC)

some large quartz grains sub-rounded to sub angular. Strong brown

7.5YR 5/6, dense

PID = 0.0 ppm [607.5/407. F]

~~545 9.0m - 8.5m~~

collect sample CC 006 B502

15:45 - 9.0m - 8.5m, 65% recovery

9.0m - 9.1m - same as 5.5 - 8.0m

at 9.1m: moist to wet clayey f-fm

sand (SC), dark grayish brown

2.5Y 4/2 (Saprolite)

at 8.3m = wet, f-fm sandy clay (CC)

medium plasticity, dark grayish

brown 2.5Y 4/2.

PID = 0.0 ppm

16:00: Begin boring #3 at location 026.

16:15: 1.0m - 2.5m.

moist, clayey f-c sand (SC)

strong brown 7.5YR 5/6,

(8)

4/11/63

with some gravel. [57G/59/53/27]  
collected sample CC02C5501

1630 2.5M - 4.0M; 100% recovery

2.5-3.5M = moist clayey fine to  
coarse sand with sand/gravel (SC)

60% G / 60% S / 30% F  
strong brown 7.54R 4/6

PIV = 60.0ppm

3.5M - 4.0M = same but olive  
57 57 4/2. Sample CC02C5501

1700 attempted sample at 4.0-5.5M -

no recovery due to 1/2 gravel  
clast in sh. will attempt again.

NO Recovery

1714: 5.1R - 7.0M 90% recovery

5.60: moist SAPPHIRE - clayey silty  
sand (SC), [60% S / 40% F]

moist color: dark greenish  
gray 5G 4/1 and yellowish

bluish 10YR 5/4.

granitic gravel at 6.0

5.0-6.5 = same but dark greenish gray  
5G 4.5/1 with some coarse  
sand.

(9)

4/11/63

6.5-9.0: moist fine sandy  
clay (CC), [15% S / 85% F]

medium plasticity - dark  
grayish brown 2.5Y 3.5/2

collected sample CC02C8502  
19:33 = 7.0-8.5M, 100% recovery

wet, high plasticity clay  
with some fine to med sand (5%)  
(CH) - dark brown 10YR 3/3

cell sand at 9.5M

Seco met 10YR 3.5/3 at 8.0M  
(dark brown)

All boring sites with bentonite chips.

French soils general description:

moist, silty brown 7.5YR 5/6,  
silty to clayey fine to coarse

sand (sand with approx 20%  
gravel and cobbles to 6" diam.)

franch depths ~ 2 meters.  
medium dense. (Fill material)

1800 Packings samples for  
shipment.

1900 Site Second, Logging Site.

66

(10) 4/2/03

0800 on site Area D.

note: All trenches excavated yesterday were backfilled prior to leaving site.

0820 & then 4 on boring #17 at location 1017.

0835 Begin drilling. Using direct-push (ps with) rig on speed mounting 2" diameter sampler fitted with acrylic tube liner.

0845: Core 1.0m 25m. Moist clayey f-c sand with some fine granules (SC) [102.6, 70.2 S, 20.2 F], strong brown 7.5 YR 5/6, Recumbent 70% granular angular, fill soils. RID 20.0 pph.

Collect sample CC017SS01.

0855 Core 2.5m - 4.0m recovery 80%. 2.5-3.0m: sand as above but yellowish brown 10 YR 5/6

3.0-3.5m = moist f-c sandy clay (C) with angular f-m granules. Strong brown 7.5 YR 5/8. Low-moist. plasticity.

4/2/03 (11)

3.5-4.0m = moist, f-c sandy clay (C) with f-m angular granules. Yellow with red 5 YR 5/8. Fill soils. (Quartzite gravel)

0915: Core 4.0m - 5.5m. Recovery = 80%.

4.0m - 5.1m = moist, f-c (A) clayey f-c sand (SC) with some

fine granules [52.6, 60.5, 35.2 F] sandy granules & f-m sub-angular to sub rounded. Looks much like upper lit but gravel inclusions indicate f-c soils.

5.1m - 5.5m = moist, clayey f-c sand. [55.2 S, 45.2 F] clay = mod. plasticity. Strong brown 7.5 YR 5/6. Fill soils

0935 Core 5.5m - 7.0m, recovery 70%.

5.5m - 6.6m = sand as 5.1m & 5.5m

6.6m - 6.7m = quartzite f-m granules

4.5 lit quartzite (GR) - dark brown

10 YR 3/3 (angular granules)

6.7-7.0m = f-c clayey sands (SC)

with f-m quartzite granules.

Strong brown 7.5 YR 5/6. (fill)

Collect sample CC017BS01.



(14)

4/2/03

1400 core 2.5m - 7.0m, Recov. = 60%  
SAME AS 4.5m - 6.0m → appears to be fill.

Collected sample CC0228502

1410 Began drilling boring 6: location 022

1420 core 0.0m - 1.0m; moist, strong  
blown 2.5 YR, medium dense, clayey  
f-c sands (SC) [60% S / 40% F]  
(fill soils)

1430 core 1.0m - 2.5m, Recov. = 80%  
SAME AS 0.0m - 1.0m. [Sample CC0228501]

1440 core 2.5m - 4.0m, Recov. 65%

SAME AS 1.0 - 2.5m  
1500 core 4.0m - 5.5m, Recov. = 80%

SAME AS 2.5m - 4.0m but more  
consolidated. Could be similar  
or may be fill. [Sample CC0228501]

1510 core 5.5m - 6.2m, Recov. 30%  
SAME AS 5.1m - 6.2m. with very  
small plant roots at 6.1m →  
ind. cobb. = fill material.  
(core short because encountered  
cobbles.)

868

1545 core 6.5 - 8.0m, Recov. 80%

(15)

4/2/03

~~SAME AS 5.5 - 6.2m~~

Moist f-c sandy clay (CC),  
low plasticity [45% S / 55% F]  
strong brown 7.5 YR 5/8 (Fill)  
becomes wet clayey sand (SC) at  
7.5m. [75% S / 25% F]  
[Sample 550228502]

1605 core 8.0m - 9.5m, Recov. = 65%  
moist to wet f-c sandy clay (CC)  
low-med plasticity [40% S / 60% F]  
strong brown 7.5 YR 5/8

1615 beyond drilling boring 7: location 028

1620 core 0.0m - ~~1.0m~~  
moist, strong brown 7.5 YR 5/8, dense,  
clayey f-c sands (SC) [60% S / 40% F]  
fill soils. (same as 9.1m core)

1630 core 1.0 - 2.5m, Recov. = 80%  
SAME AS 0.0 - 1.0m with 15% gravel (S)  
[15% G / 55% S / 30% F] (SC) (Fill)

1640 core ~~2.5m - 4.0m~~, Recov. 90%  
SAME AS 0.0 - 1.0m with trace  
fine gravel. (Fill)

At 3.5m becomes f-c sandy  
clay (CC) [20% S / 80% F]

(16)

9/2/03

Low plasticity, strong brown  
 7.5 YR 4.5/6 (F, 8C)  
 16.55 core 4.0m - 5.5m, 90% Recov.  
 4.0m - 4.3m = Sand at 3.5 - 4.0 m  
 4.3m - 5.5m = moist clayey f-c  
 sand (SC) [65% / 35% F]  
 Strong brown 7.5 YR 5/6 (Fill)  
 dens. [Sample CC028B501]  
 1804: core 5.5m - 7.0m, 40% Recov.  
 moist, clayey f-c sand (SC) (Fill)  
 [55% S / 45% F] Strong brown  
 7.5 YR 4.5/6

869

At 6.6 - 6.9 m = root inclusions  
 color changes to dark brownish  
 gray 5G 4/1 + fine angular  
 quartzite gravel.  
 1825 core 7.6m - 8.5m, 65% Recov.  
 moist f-c sandy clay (CC)  
 [45% S / 55% F] strong brown  
 7.5 YR 4.5/6 with some  
 dark greenish gray 5G 4/1  
 at 9.0 - 9.2 m

[Sample CC028B502]  
 1830 Leaving Site



66

(17)

4/3/03

2051k 0745 - Area D.  
 Begin drilling boring at location 027  
 0750: core 0.0 - 1.0m, 100% Recov.  
 moist, clayey f-c sand (SC) J.  
 with some thin - medium gravel.  
 [57% G, 43% S, 20% F], dark yellowish  
 brown 10 YR 4.5/6 (Fill sand)  
 0755 core 1.0 - 2.5m, Recov. = 40%  
 moist, f-c sandy clay (CL)  
 low plasticity [40% S / 55% F]  
 yellowish red 5 YR 5/8  
 0811 core 2.5m - 4.0m, Recov. = 60%  
 moist, f-c sandy clay (CC)  
 low med. plasticity [60% S / 60% F]  
 strong brown 7.5 YR 4.5/6  
 0815 core [Sample CC027B501]  
 3.5 - 4.0 = compact, moist f-c sandy  
 clay (CL) med. plasticity [40% S / 60% F]  
 dark greenish gray 5G 4/1 +  
 high mica content (microclay)  
 depending on some sandy clay (CL)  
 at 20.2 m [80% F], red white  
 filling (CC) (microclay)  
 0820 core 4.0 - 4.5m, 20% Recov.

(18)

4/3/03

(encountered cobbles (quantized))

moist, sandy clay (cc)  
medium plasticity - ~~very~~

~~low plasticity~~ - s.p.m.

unimodal greenish gray 55-6/1  
and olive 57 64.5/4

08:19 cap 50-6.5% Recov. 55%

moist f-m sandy (cc) clay (cc)

mod. plasticity. micaceous

(not - mucous)

unimodal olive 57 4/3

reddish brown 57R 5/6, and

yellowish brown 10YR 5/8.

[Sample CC0278502]

09:05 cap 65% - 7.0% Recov. 50%

applesite - ~~tan~~ angular granular,

highly weathered f-ls, phs - clay.

lots mica, some manganese.

moist f-m sandy clay (cc)

low plasticity. unconsolidated

7.5 YR 6/10 to 10YR 6/6

reddish yellow to brownish

yellow.

07:30 parking up site to house to Area 41.

(19)

4/3/03

09:45 Leaving Area 41

09:55 on site Area 41

locating sample areas

10:41. Wght Level BW14 = 6472M 70c

→ well located in adjacent zone near

107 and 108 original storage sites.

100's meters between these sites

ground surface.

11:05 boring & well locations marked.

11:30 Lunch Break

12:15 On site - waiting for

utility clearance.

13:30 Boring drilling / st boring

at sites 41. - Location = 05B

13:40 capy 0.0m - 1.0m Recov. = 70%

material in core looks like

decomposed granite - applesite -

can see small structures of

with touching quartz & feldspar with

60-like shape and other minerals.

when crushed fragments disintegrate

to chips - and material becomes:

6025/442 FJ = strong brown

4/3/03

1350 0.5 YR 4.5/c dense

1700 Core 1.0 - 2.5 m, recovery = 90%,

SAM AT 0.0 - 1.0 m Sat. A=0

Recoverable. Core = 9.5 YR 5/6.

[Sample at 0.2 - 1.5 m = CC052SS01]

1400 Core 2.5 - 3.0 m, recovery = 90%

difficult drilling / recover at 3.0 m

SAM AT 1.0 - 2.0 m.

1410 Begin 2nd boring at location 061.

1420 Core 0.0 - 1.0 m, recovery 60%

0.0 m - 0.5 m = Fill materials;

moist, Red 2.5 YR 7/6, f.c

Sandy clay (sc) and yellowish Red

5 YR 4/6 clay clay f.c

Sand (sc) - medium, appears to

be decomposed granitic source, some

porphyry.

0.5 m - 1.0 m; combined at 0.5 m

with Saprolite = same as boring

052 - granitic structure visible

1430: Core 1.0 - 2.0 m, recover = 90%

SAM AT 0.5 - 1.0 m, but more

recoverable. [Sample CC061SS01]

1440: changes to percussion bit to

4/3/03

Advance boring. Sample collected

from cutting at 4.0 - 5.0 m;

see 061SS01; Saprolite.

1505 Boring seal: Location 062

0.0 - 1.0 m sam.

0.0 - 0.1 = fill soil as before.

0.1 - 1.0 = Saprolite (granitic)

no M.C. 10 YR 8/4 pink, light brown

to 10 YR 5/4 yellowish brown

Sample CC062SS01

1510 Boring 4th. Location 065

core 0.0 - 0.3 m -

0.0 - 0.3 = Fill: some dark staining (0.3)

0.3 - 0.3 = Saprolite: strong brown

9.5 YR 5/6, dense.

1520 core 0.7 m - 1.5 m = Saprolite

AS 0.3 - 0.7 m.

Sample combined 0.3 m - 1.5 m

CC0658J01

Boring 5 -> Location 060

1530 Core 0.1 m - 0.8 m = fill soil ->

1.5 m thick sand with granitic at 0.7 - 0.8

(sc)

(22)

4/3/03

Strong brown 7.57R 5/6.

1540i core - 0.8 - 1.5 m.

0.8 - 0.9 = same as above. (SC)

0.9 - 1.2 = sil - red 2.57R 4/6

1.2 - 1.5 fine - med sandy clay (CC)

1.2 - 1.5 m = water seal

Silt (MC) brownish yellow

1.07R 6/5. Fine shaly

silt with manganese carbonate

1545: core 1.5 m - 2.2 m - silt (MC)

same as above.

combined cores for 2 samples:

0.1 - 1.2 = CC0608501

1.2 - 2.2 = CC0608501

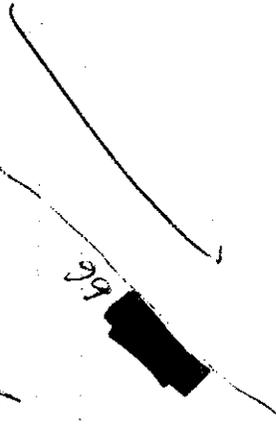
1608: core 2.5 m - 4.0 m, recover = 100%

= silt (MC) - same as above.

1425 Area Secured - Leaving Area 41

1530 Leaving Area D. After parking

Sample 61



(23)

7/4/03

08:30 Onset Area 41

09:00 continue down my 0 (20)

with 4.0 m - 4.7 m =

same as above but good

same clay - low plasticity (ML)

09:10 Move to boring location 063

core 0.1 - 0.8 m [sample CC058501]

0.1 - 0.6 = fill material - DG (SC)

0.6 - 0.8 = fill material - clay

gms wts. (GC)

09:18: core 0.8 - 2.3 m Recover 70%

Sample (DG), white weather

= marsh clay, s.c. sand

with some large gravels (SC)

[52 g / 95 g / 20 g] [Sample 7]

Strong brown 7.57R 4.5/6

09:25 1.1 - 2.0 m: Bore 7, length 0.58

core 0.1 - 0.8 m: F.A. material

1.1 - 1.5, 8-12 sandy clay (CL)

Low plasticity red 2.57R 4/6

09:35: Core 0.1 - 0.4 m, recover = 100%

0.8 - 1.1 m: same as above

1.1 - 2.4 m: high weathered argillite

black (Sample 61) yellowish brown

Sample 0.8 - 1.4 m - CC0585501

Sample 1.4 - 2.4 m - CC0588501

(24)

4/4/03

107R 5/6, envelopes to clay  
8-a sand (SC) [5523/45% F]

0988 Now to bring #8 Log to 0.5C

0950 core 0.1-0.8m = weathered

quantity - AS bring 50 (1.2m)

sample CC 0.563501

core 0.1-2.3m = highly weathered

quantity (54 samples)

Stacy Green 7.5YR 4.5/6

1000 Now to bring #9, look 55

core 0.1-0.8m = fill in 1000

core 0.1-2.3m = brown = 60%

sample #14 #50

1010 Now to bring #13, look 0.51

core 0.1-1.0m = fill soil

0.1-0.6m = weathered quantity fill

0.6-1.0m = fill - clay (Ct/Ck/H)

med. high plasticity & dark

brown 1.0YR 4.5/3 [E6051550]

organic residue at 1.0m = wood

1015 core 1.6-2.3: Saps (Lk. at 1.3m)

1030 Now to bring #11, look 0.57

core 0.1-0.8m = Saps (Lk)

(25)

4/4/03

Stacy Green 7.5YR 4.5/6

sample CC 0.5755 at 0.1-1.3m

core 0.1-2.0m = Saps at 1.5m

1045 Now to bring #12, look 0.64

core 0.1-0.8m = Saps (Lk)

(weathered quantity fill)

quantity volume at 0.1-0.4m

Stacy Green 7.5YR 5/6

(void samples)

Now to bring #13, look 0.559

1050 core 0.1-1.0m = fill soil

(low weathered quantity fill)

1.5 YR 5/6

1100 core 0.8-2.4m = Saps (Lk)

(quantity)

sample 0.1-1.6m [CC 0.595301]

1200 used blocks

1300 Set up on bring #14, look 0.67

1305 core 0.1-0.8m = fill soil

med. f-c sandy clay (CC) [E6051550]

Stacy Green 7.5YR 4/6 [E6051550]

1315 core 0.8-2.2m = Saps (Lk) very 70%

0.8-2.0m = fill (CC) [CC]

2.0m-2.2m = Saps (Lk)

4/14/53

13:27 core 2.2m - 4.0m = Saprolite  
very weathered

13:40 core 0.1m of 0.8m = Saprolite, location 068

core 0.1m - 0.3m = Sll (cl)

0.3 - 0.8m = Saprolite

13:48 core 0.8m - 2.2m = Saprolite

Bove to boring #16, location 069

14:00 core 0.1m - 0.8m = Sll [Sampled]

14:08 core 0.8 - 2.2m = Saprolite  
Sample

Bove to boring #17, location 070

14:16 core 0.1 - 0.8m = Sll

14:28 core 0.8 - 2.2m

0.8 - 1.5m = Sll [Sampled]

1.5m - 2.2m = Saprolite

note: upper 30cm of 0.8-0.1m

0.8 core colon = dark grayish  
gray 5.6.4 4/11

(2)

4/8/53  
Onsite Area D 08:00

Start drilling @ location 24.

Will utilize HSA & AIR  
Rotary as needed per

Drilling using CME Drill Rig  
& water + superflow, saw size 4  
wipers

1050 Borehole installed to 45'  
continuous core to 4'

@ 15' 49' 2' sample  
every 5'. Let well set 4L

After lunch ML @ 37'

12:15 ML @ 37' install well, 2x  
20' bore casing

14:05 Borehole seal installed mobilize  
to location #11 & start drilling

Now starting drilling 001 @ 10'

(32)

ARRIVE W/ SET UP ON LOCATION #54  
COLLECT SURFACE SOIL SAMPLE @ 10L

1600 HRS #54 @ 35, ESTIMATED  
REPAIR WITH AUGER FSP  
NEAR SWITCH TO ROCK COREING  
ARRIVE W/ IS RETURNED @ 1630, WORK  
MUST STOP @ 1600.

OA FED HAS RUBBER FROD WITH RIG  
(WATCH) MUST NOT BE ABLE TO AUGER  
FURTHER. WILL LET SITE S.T. &  
CHECK W/L THURSDAY

1630 OFF SITE.

COLLECTED SAMPLES

CC-001 BS-002  
CC-002 054 BS-001  
CC-054 BS-002

LEWIS JENY  
1/16/03  
2/1/03

(31)

4/10/03

ARRIVE MW 1, 8.14 AM @ 0830 (REL)  
MW 24, 8.30 AM @ 0835 (REL)

0730 ON-SITE PREP. EQUIP  
0800 FED CHECKS WL, NO WATER  
SA BUT AUGER BIT IS MUST-WET  
OPTION 3 A: SWITCH TO COREING  
B: SWITCH TO SAMPLED VIA  
AUGER.

0830 OFF. TO TRY SAMPLE AUGERS  
BEARING @ 35'.  
0900 FED RETURNED AUGERS, WORKING  
ON RIG

0930 MAKE BREAK.  
0945 START DRILLING. FOD ESTIMATED  
WL @ 36' NOW USING AUGERS  
MWS @ 45' WL @ 44'. ~~GOOD~~ ESTIMATED  
WL WILL BE BOUND TO ~36'  
DUE TO INTRUSIVE ACTIVITY & FRACTURE  
WL @ 40' AFTER 5 MIN. WILL  
WAIT FOR WL TO STABILIZE OTHER  
BEFORE CUT BEARING WITH 3" AUGER  
& INSTALL WELL

ML @ 37 @ 11:00, FED WILL REMOVE  
ADAPTER & PREP FOR REMAINING.

1145 LUNCH

1300 RESUME WORK. FED START REMAINING  
CUT BOREHOLE TO 8" DIA.

ML @ 36 @ 1300

1630 NEW INSTALLED BOREHOLE COMPLETED  
TO 145' WILL GREAT REMAINING

4110'S FED TESTS UP ON 1200

"36" NOTED THAT SELECTED LOC  
WAS WITHIN 10'S OF OVERHEAD UTILITIES  
INSTALLED FED TO MAKE USE STRAPSIDE  
OF OVER HEAD LINES BECAUSE OF  
SAFETY CONCERNS.

MINIMAL  
AED, SAMPLES COLLECTED TODAY.

*Handwritten signature*  
AUBURN  
10/10/88

4110'S CAMP CARROLL AREA 41

0730 ON-SITE PREP TO START  
BORING #66. NOTE CONDITIONS  
ARE COLD & RAINY

0800 AIR IN USE FED, INDICATES  
THAT THE DRILLERS WILL  
START THIS BORING USING 6"  
HSA. IF SITE CONDITIONS ALLOW  
THE WELL WILL BE INSTALLED  
IN THE OPEN 6" BOREHOLE. IF  
HSA COLLAPSES TO LESS THAN  
REQ D. BORING WILL BE REMOVED  
WITH 3" HSA.

1130 MINIMAL SAMPLES REQUIRED DUE  
TO PROTECT DEFUSAL PILE BARE  
TO 45' & CHECK ML / COLLECT  
SPRINTXON SAMPLE.

1230 LUNCH

1330 RESUME WORK.

1435 SAMPLER REFUSED @ 45'. NO WATER  
ENCOUNTERED, FED DECIDES TO PULL  
TO 50' & RECHECK ML.

(35)

4/2/03 CAMP CARROLL AREA D

0730 INSURE, SOMMY, CLEAR,  
SIT UP ON LOCATION # 37  
@ AREA D.

0810 START PUMPING

0900 NOTED CHEMICAL CODE @ N20 - 30'

1045 BUREAU # 37 COMPLETE, WELL INST  
TO FOLLOW (2 ANALYTICAL PAMP. COLLECTED)

1145 WELL INSTALLED (FILTER PICK & BENT  
SEAL

1200 LUNCH BREAK

1300 RESUME WORK SETUP ON LOC # 39  
GREAT MUD # 57

1605 BUREAU # 39 COMPLETE TO 4'  
INSTALL WELL 4/12/03.  
NOTE LOC # 38 NO ACCESS THIS  
WEEKEND MUST ALL ON MUD / TIES  
TO TIES WELL: INSTALL # 39, BENT /  
INSTALL # 12.

(34)

1140 @ 50' SAMPLE RETURN

ML @ 50' @ 144, @ 45, 145

1700 BENT WELL COMPLETE  
DECIDED TO USE 25' SECTION DUE  
TO SLOW DEPOSIT OF BENT  
PROJECT BEHIND RISE TO LOC  
54 IN 2.35, 30 AREA SURF  
ROAD COVER WERE ALSO.

COLLECTED SAMPLES:  
CC-066 SB-01  
CC-066 SB-02  
CC-066 SB-03.

NOTE: PTD CREW WILL DOWN 300  
FOR WEEKEND. MR. KIM WILL BE  
THE PRIMARY POC. WILL DRILL  
AREA D BECAUSE AREA C1 WILL BE  
SECURED OVER THE WEEKEND.

4/12/03  
LA-30  
b6

37

4/21/07 CAMP CHANGE AREA D R1

0730 ON SITE W/ CATER IN # 59  
BEGAN WORK INSTALLATION.

0815 INSTALLATION COMPUTERS  
SET UP ON LOC #12

1105 BOONE COMPLETE TO 41'  
R.O LUNCH BREAK,

1200 RESUME WORK

1403 WELL # 2 R INSTALLED. (FIELD PACE  
& SOIL) INSTALLING GROUT.  
NOTED THAT 10W COTINGS ARE  
BEING BAGGED 1 FT DEEP FOR

TRANSFERT TO LAND FARM FACILITY  
NEAR AREA D (ADJACENT TO  
SHANE ANNA RANGE.) COTINGS  
FROM AREA D WELLS #1, 24  
WERE "DISPOSED OF" ~~SHANE~~ BACKFILLED  
DURING TRENCHING INVESTIGATION  
NEAR # 1 @ AREA D.

1500 SAMPLES IN AREA D WILL BE  
COLLECTED FROM AREAS WITH

COLLECTED ANALYSES SAMPLES

CC-03765-01

CC-03788-02

TODAY NO SOIL COLLECTED

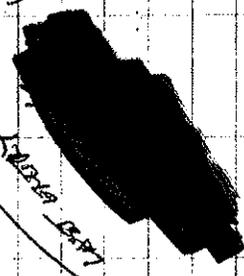
PROB #3A.

1005 DEEPER SOE

4/21/07

878

LABOR COST



NEEDED OPR OBSERVABLE IMPACT.  
NO ANALYTICAL SAMPLES COLLECTED  
TODAY. WORK WILL RESUME @  
AREA # 38 OF AREA #01 #53.

10

~~REDACTED~~

ALLEN  
SUPERVISOR

879

(39)

4/14/68 CAMP GREEN AREA D #41 B1

0700 CASING AREA D SAW SINK RELOCATED  
LOCATION #38 FROM THE BOTTOM OF THE  
HILL TO AN AREA LOCATION 30M  
NORTH OF #57. THIS CHANGE  
IS DUE TO SUSPECTED CONTAMINATION  
TO  
IN LOCATION #57. I NOTED THAT  
SAW SINK THAT THIS CHANGE WILL  
LEAVE NO BENTONITE INTO BR AT  
ELEV. BELOW AREA D HOWEVER  
THE LENGTH TO IS IF COST IS  
ENCOUNTERED IN #57, THIS COST / AREA  
MAY EXCEED OUTSIDE OF AREA D.  
DR. LEE ~~RECENT~~ MADE THIS DECISION  
TO RELOCATE # 38.

0805 START BENTONITE #38, AREA D.

0900 MATING MATERIAL ENCOUNTERED @  
TUNNEL IN BENTONITE INCREASINGLY  
DENSE WITH DEPTH, FUD SWITCH TO  
6" AUGERS.

40

1100 @ 1/2" horizontal is very porous. Fed

thinner. Mr. Juma indicated that he cannot penetrate with 6" HSA

FED will use coring to corer the base. Set up coring equip

1130 Lunch break

1132 Re-spike work. Note: FED is using water as a circulation fluid. It will skew GW levels in the

local vic. GW measures might stand be. Trench after GW levels have stabilized.

1150 Well instructed. Mobilize to collect 601. If boring is completed, will return to collect a sample. Boring well # 37

1222 Inside area 41, screen # 50

1150 #53 complete to W. [Redacted]

1230 [Redacted]

1230 [Redacted]

1230 [Redacted]

1230 [Redacted]

1230 [Redacted]

1230 [Redacted]

4/15/03

CAMP CAMP AREA PT AREA 41

0710 WASTE AREA 41, LOCATION # 53

W/ DATA FROM LOC # 46 INDICATE W/ SHOULD BE ABOUT 30' DEPTH.

NOTED THE PRESENCE OF A OPEN PITTING TRENCH, AND THE SIZE OF THE PITTING LIST THAT IT

DEPTHS. THE HIGHER W/ MAY BE A RECHARGED ZONE, OR A LEVEL OF

W/ THAT BE INFILTRATING TO THE

30' W/ OR A CONTAINED LAYER INDICATED

TO BE SET W/ # 40 BUT SCREEN TO 10' (30' SCREEN SECTION) TO CAPTURE

ALL PESTICIDES

LOCATION # 53 COMPLETE. MOBILIZE

BACK TO AREA "D" TO COLLECT SUB-SURFACE

SOIL SAMPLE

ON SITE AREA "D" SET UP ON LOC #

40

LUNCH BREAK @ 17' IN LOC # 40

RESUME W/ W/

1230 NATIVE MATERIAL ENCOUNTERED

UNSATURATED 2 ANALYTICAL SAMPLES

FURDAN

CC-040 BS-01

CC-044 BS-02

1305 AND COMPLETE K10 WELL (MISPLACED)  
BEING BACK FILL WITH BENTONITE  
+ SAND.

18/8

## **Appendix C**

Boring Logs, Well Completion Diagrams, Well Development Logs,  
and Groundwater Sampling Logs

Soil Sampling PID Checking AREA D

Point NO/ Soil NO.	Date	Time(1st sampling)		Depth	PID (ppm)	REMARK	Date	Time(2nd sampling)		Depth	PID (ppm)	REMARK
		Collected Time	Measured Time					Collected Time	Measured Time			
CC001 BS01	2003.04.01	11:03	-	1m	-	ascon at 9H	2003.5.27	11:05	-	1m	-	
	2003.04.09	8:25	8:45	20-22H	57.6		2003.5.27	12:15	-	6.6m	-	
		8:35	8:50	25-27H	465							
		8:55	9:20	35-37H	16.1							
		9:20	9:45	40-42H	N.D							
CC003 SS01	2003.04.01	14:40	14:58	2m	N.D		2003.6.2	10:31	10:50	1-2.2m	0	
CC004 SS01	2003.04.01	16:53	-	1m	-		2003.5.27	13:55	-	1m	-	
CC006 SS01 BS01 BS02	2003.04.01	14:29	-	1-2.5m	-		2003.5.28	15:10	-	2-3m	-	
		15:00	-	4-5.5m	-	15:28		-	3.5-4.5m	-		
		15:15	-	5.5-7m	-	15:52		-	5-6m	-		
CC007 SS01	2003.04.01	11:15	11:27	2m	0.1		2003.6.2	10:59	11:15	1-2.2m	5.1	
CC008 SS01	2003.04.01	11:30	11:45	2m	0.1	BG=0 mg/l	2003.5.28	14:12	14:35	2-3m	0	
CC009 SS01	2003.04.01	11:45	12:00	2.1m	0.2		2003.5.28	14:40	-	2-3m	-	
CC010 SS01 BS01 BS02	2003.04.01	10:28	11:02	1m	0.2		2003.5.27	14:20	-	1-2m	-	
		11:40	-	4.7-5.8m	-	15:30		-	4.7-5.8m	-		
		12:20	-	7.3-8.6m	-	15:56		-	7.3-8.6m	-		
CC012	2003.04.13	9:35	10:00	0-2H	N.D							
		9:45	10:00	2-4H	N.D							
		9:50	10:10	4-6H	2.6							
		10:00	10:20	6-7.5H	2.3							
		10:05	10:40	8-10H	40.6							
		10:10	10:40	10-12H	7.4							
		10:15	10:45	12-14H	453							
		10:20	10:45	15-17H	40.7							
		10:25	10:50	20-22H	236							
		10:50	11:20	25-27H	8.1							
		11:05	11:25	30-32H	284							
		11:25	12:15	35-37H	5.5							
		11:45	12:15	40-42H	6.6							
CC013 SS01	2003.04.01	12:00	12:15	2m	0.5		2003.5.27	14:48	-	2-3m	-	
CC014 SS01	2003.04.02	14:00	-	1.9m	-		2003.6.2	11:22	11:35	1-2.2m	0	
CC015 SS01	2003.04.01	14:20	14:55	2m	N.D	T.P: 68.1, lots of ascon	2003.5.28	12:25	12:40	2-3m	0	
CC017 SS01 BS01 BS02 BS03	2003.04.02	8:43	9:13	1-2.5	N.D		2003.6.2	13:05	13:30	1-2.2m	2.5	
		8:55	9:15	2.5-4m	0.1	15:16		15:40	4-5.2m	2.6		
		9:35	10:40	5.5-7m	0.8	16:15		16:40	5.5-6.7m	1.2		
		9:55	10:47	7-8.5m	0.7	16:15		16:50	7.0-8.2m	2.7		
CC018 SS01 BS01 BS02	2003.04.02	11:10	-	1-1.25m	-		2003.6.2	16:58	17:20	1-2.2m	2.9	
		13:20	13:40	4.5-6.0m	1.3	17:13		17:40	4.5-5.2m	3.4		
		14:00	14:18	7.5-9m	0.2	17:46		18:10	7.5-8.2m	5.1		
CC019 SS01	2003.04.01	15:15	15:29	1.2m	0.1		2003.5.27	17:57	-	1.2-2.2m	-	
CC020 SS01	2003.04.01	16:20	16:35	2m	N.D		2003.5.29	15:56	16:15	1.5-2.5m	5.3	
CC021 SS01	2003.04.01	16:58	17:15	1.9m	N.D		2003.5.29	15:36	15:50	1.5-2.5m	4.1	
CC022 SS01 BS01	2003.04.02	14:30	-	1-2.5m	-		2003.6.3	9:10	9:40	1.0-2.2m	3.4	
		15:45	16:05	6.5-8m	0.1	10:20		10:36	6.5-7.7m	0.7		
CC023 SS01	2003.04.01	17:15	17:23	2m	N.D		2003.5.27	17:02	-	2-3m	-	
CC024 BS01 BS02 BS03	2003.04.08	9:50	10:05	20-22H	83.8		2003.6.2	18:20	18:40	5.5-6.7m	2	
		10:30	10:52	30-32H	1603	18:40		19:40	8.5-9.7m	3.5		
		10:40	11:10	35-37H	325	19:20		19:50	9.7-10.8m	0		

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Point NO/ Sol NO.	Date	Time		Depth	PID (ppm)	REMARK	Date	Time		Depth	PID (ppm)	REMARK	
		Collected Time	Measured Time					Collected Time	Measured Time				
CC039	2003.04.12	14:05	14:25	8-10ft	N.D								
		14:10	14:30	10-12ft	N.D								
		14:15	14:40	15-17ft	N.D								
		14:27	15:00	20-22ft	N.D								
		14:45	15:10	25-27ft	N.D								
		15:25	16:00	30-32ft	N.D								
		15:35	16:00	35-37ft	N.D								
CC040	2003.04.15	10:30	10:55	0-2ft	42		2003.5.29						
		10:35	10:55	2-4ft	22								
		10:45	11:05	4-6ft	14.7			11:48	12:10	1.2-2.2m	4.8		
		11:05	11:35	6-7.5ft	3.2								
		11:15	11:35	8-10ft	8.8								
		11:20	11:35	10-12ft	106								
		11:25	11:40	12-14ft	190								
		11:30	11:40	15-17ft	72.1								
		BS01	13:15	13:30	20-22ft	94.7			13:22	13:33	6-6.7m	4.3	
			13:20	13:35	25-27ft	26.5							
			13:40	13:50	30-32ft	5.4							
CC080	BS01	2003.04.09	10:40	-	4.5m	-	2003.6.3	11:45	12:00	4.5-5.7m	1.4		

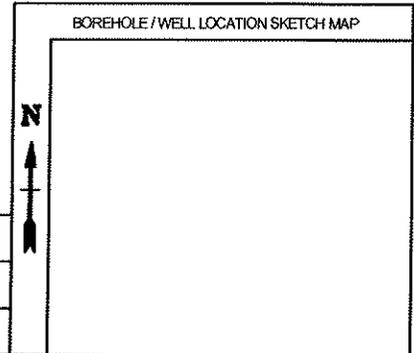
885



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Point NO./ Soil NO.	Date	Time(1st sampling)		Depth	PID (ppm)	REMARK	Date	Time(2nd sampling)		Depth	PID (ppm)	REMARK	
		Collected Time	Measured Time					Collected Time	Measured Time				
CC066 SS01	2003.4.11	8:30	8:53	0-2ft	113		2003.6.4	10:05	10:20	0.5-1.7m	6		
		8:30	9:05	2-4ft	53.6								
		8:40	9:10	6-7.5ft	44.6								
		8:45	9:20	8-10ft	15.2								
		BS01	8:50	9:20	10-12ft	2			10:35	10:48	3-4.2m	4.1	
			9:05	9:30	12-14ft	1.8							
			9:45	10:15	15-17ft	9.5							
			10:05	10:40	20-21.5ft	25.3							
			10:30	10:50	25-27ft	30.2							
		BS02	11:05	11:30	30-32ft	6							
			11:35	12:05	35-35ft*	5.9			11:25	11:50	9-10.0m	0.5	
		CC067 SS01	2003.04.04	13:05	13:35	0.1-0.8m		0.8		2003.6.4	12:15	12:40	0.5-1.7m
CC069 SS01	2003.04.04	14:00	14:35	0.1-0.8m	0.2	T.P.:23.3 CO2:1831							
CC070 SS01	2003.04.04	14:16	14:38	0.1-0.8m	0.1	T.P.:30.2 CO2:5300.2							

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# LOG OF WELL AREA 41 #53

PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/14/03 15:22</b>		
LOGGED BY <b>[Redacted] b6</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/15/03 09:00</b>	
DRILLING CONTRACTOR / DRILLER <b>FED / [Redacted] b6</b>	DRILLING METHOD <b>Hollow-Stem Auger</b>		COORDINATES
SAMPLING METHOD <b>Split-Spoon Sampler</b>	SAMPLE HAMMER TYPE <b>Hydraulic Hammer</b>	SIZE / TYPE OF BIT <b>6"</b>	SURFACE ELEVATION <b>mean sea level</b>

WELL INSTALLED? YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	CASING MATERIAL / DIAMETER <b>Sch 40 PVC / 2"</b>	SCREEN Type: <b>Slotted</b> Material: <b>PVC</b> Length: <b>6.1 m</b> Diameter: <b>2"</b> Slot Size:				
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE <b>4/15/2003</b>

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
		4/4/67	0.6098 / 83					SC	[Hatched Pattern]	CLAYEY SAND (SC): reddish yellow(7.5YR 6/6), ~70% medium to coarse sand, ~30% fines, moist; medium dense.			PVC Top Cap
1		5/9/10/12	0.6098 / 88					SM	[Dotted Pattern]	SILTY, CLAYEY SAND (SM): reddish yellow(7.5YR 6/6) 30% grades to light brown(7.5YR 6/3), ~70% sand, ~30% fines, dense.		1	1/2" Dia. Bentonite Pellets
2		2/12/16/22	0.6098 / 100									2	
3		18/23/25	0.6098 / 67									3	
4		9/26/37/50	0.6098 / 52									4	
5		5/40/41/50	0.6098 / 87					CL	[Diagonal Lines]	SILTY, CLAYEY SAND (CL): light yellowish brown (10YR 6/4), ~20% very fine to fine sand, ~80% fines, moist.		5	
6		6/40/45/50	0.6098 / 91					SM	[Dotted Pattern]	SILTY SAND (SM): reddish yellow(7.5YR 6/6) 40% grades to reddish yellow(7.5YR 6/6), ~70% medium to coarse sand, ~30% fines, wet; very dense; increased sand at 9.1 meters bgs (80% sand, 20% fines)		6	
7		31/50	0.6098 / 100									7	Filter Pack
8		50	0.1524 / 100									8	Slotted PVC Casing

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41.GPJ ACE 1836.GDT 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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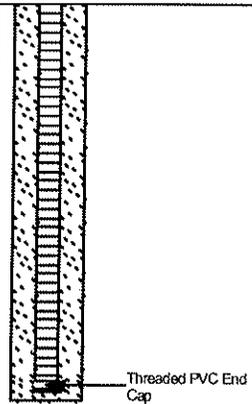
BOREHOLE / WELL LOCATION SKETCH MAP



# LOG OF WELL AREA 41 #53

PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/14/03 15:22</b>
LOGGED BY <b>[Redacted]</b>	DATE & TIME FINISHED <b>4/15/03 09:00</b>
REVIEWED BY	

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
10		47	0.1524				10		[Stippled pattern]			10	
11							11		[Stippled pattern]			11	
12							12		[Stippled pattern]			12	
13							13					13	
14							14					14	
15							15					15	
16							16					16	
17							17					17	
18							18					18	
19							19					19	
End of Borehole at 12.2 m.													

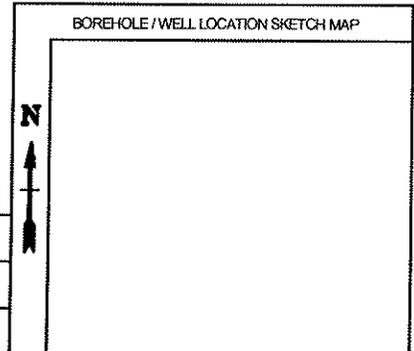


BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41.GPJ ACE\_18356.GDT 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF WELL AREA 41 #54



PROJECT NO.		PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>	
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>		DATE & TIME STARTED <b>4/9/03 13:40</b>	
LOGGED BY <b>[Redacted]</b>	REVIEWED BY <b>[Redacted]</b>	DATE & TIME FINISHED <b>4/10/03 14:05</b>	
DRILLING CONTRACTOR / DRILLER <b>FED / [Redacted]</b>		DRILLING METHOD <b>Hollow-Stem Auger</b>	COORDINATES
SAMPLING METHOD <b>Split-Spoon Sampler</b>	SAMPLE HAMMER TYPE <b>Hydraulic Hammer</b>	SIZE / TYPE OF BIT <b>8"</b>	SURFACE ELEVATION <b>mean sea level</b>

WELL INSTALLED? YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	CASING MATERIAL / DIAMETER <b>Sch 40 PVC / 2"</b>	SCREEN Type: <b>Slotted</b> Material: <b>PVC</b> Length: <b>6.1 m</b> Diameter: <b>2"</b> Slot Size:				
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE <b>4/10/2003</b>

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41.GPJ ACE: 1.836.GDT 18/9/03

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		WELL CONSTRUCTION DETAILS	
										LITHOLOGIC DESCRIPTION			
0		1/3/54	0.6098 / 70	CC-054SB-01		SS	0	SC	[Hatched Pattern]	SANDY LEAN CLAY (SC): greenish gray (GLEY1 5/5GY), ~10% gravel, ~30% sand, ~60% fines, loose.		0	PVC Top Cap
1		2/3/6/10	0.6098 / 80				1	SC	[Hatched Pattern]	CLAYEY SAND (SC): strong brown (7.5YR 4/6) 50% grades to reddish yellow (7.5YR 6/6), ~50% medium to coarse sand, ~50% fines, loose.		1	
2		7/9/11/15	0.6098 / 90				2	SC	[Hatched Pattern]	CLAYEY SAND (SC): strong brown (7.5YR 5/8), ~60% coarse sand, ~40% fines, loose.		2	
3		8/11/14	0.4573				3	SC	[Hatched Pattern]			3	
4		10/15/15/18	0.6098 / 70				4	SC	[Hatched Pattern]	CLAYEY SAND (SC): light reddish brown (5YR 6/4) 40% grades to brown (7.5YR 5/4), 60% coarse to medium sand, ~40% fines, moist, medium dense.		4	
5		4/12/15/20	1.2195 / 80				5	SM	[Dotted Pattern]	SILTY SAND (SM): pink (7.5YR 7/3), ~70% coarse to medium sand, ~30% fines, dense.		5	1/2" Dia. Bentonite Pellets
6		4/24/29/33	0.6098 / 70				6	CM	[Dotted Pattern]	SILTY SAND (SM): reddish brown (5YR 5/3) 50% grades to reddish brown (5YR 5/4), ~70% coarse to medium sand, ~30% fines, dry; very dense; increased clay content at 7.6 meters bgs (80% sand, 40% fines).		6	
7		8/20/49/50	0.6098 / 100				7		[Dotted Pattern]			7	
8		25/50	0.3049 / 100				8		[Dotted Pattern]			8	

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BOREHOLE / WELL LOCATION SKETCH MAP



# LOG OF WELL AREA 41 #54

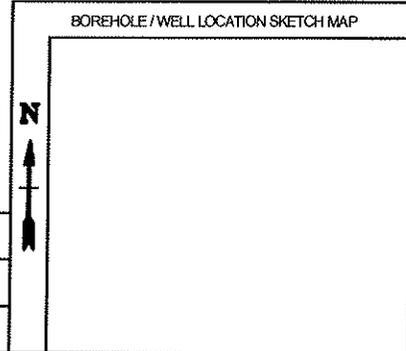
PROJECT NO.	PROJECT NAME
<b>Camp Carroll Area D and Area 41 RI</b>	
LOCATION	DATE & TIME STARTED
<b>Camp Carroll, Taegu, Republic of Korea</b>	<b>4/9/03 13:40</b>
LOGGED BY	DATE & TIME FINISHED
<i>bl</i>	<b>4/10/03 14:05</b>
REVIEWED BY	

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:	LITHOLOGIC DESCRIPTION	DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
10		16/4350	0.4573 / 100	CC-054SB-02	X	SS	10	SM			SILTY SAND (SM): reddish brown(5YR 5/3), ~60% coarse to medium sand, ~40% fines, very dense.	10	Filter Pack
11		40/50	0.3049 / 0				11				Preprobe. No recovery.	11	Slotted PVC Casing
13		50	0.1524 / 100				13	SM			SILTY, CLAYEY SAND (SM): yellowish brown (10YR 5/4), ~60% coarse to medium sand, ~40% fines, no odor; wet; very dense.	13	
14							14				End of Borehole at 13.7 m.	14	Threaded PVC End Cap

BORING LOG METRIC UNITS. CAMP CARROLL AREA D AND AREA 4 - GPJ ACE - 1836.GIT - 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF WELL AREA 41 #66

PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/11/03 08:15</b>		
LOGGED BY <b>[Redacted] bb</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/11/03 16:30</b>	
DRILLING CONTRACTOR / DRILLER <b>FED / [Redacted] bb</b>	DRILLING METHOD <b>Hollow-Stem Auger</b>	COORDINATES	
SAMPLING METHOD <b>Split-Spoon Sampler</b>	SAMPLE HAMMER TYPE <b>Hydraulic Hammer</b>	SIZE / TYPE OF BIT <b>6"</b>	SURFACE ELEVATION DATUM <b>mean sea level</b>

WELL INSTALLED? YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	CASING MATERIAL / DIAMETER <b>Sch 40 PVC / 2"</b>	SCREEN Type: <b>Slotted</b> Material: <b>PVC</b> Length: <b>6.1 m</b> Diameter: <b>2"</b> Slot Size:				
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE <b>4/11/2003</b>

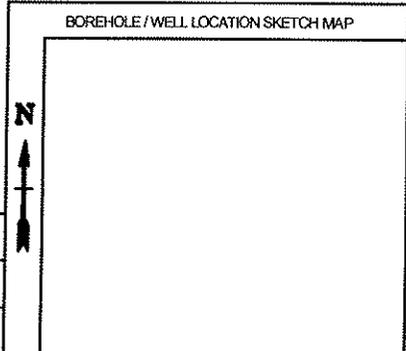
DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
0		2/4/4	0.6098 / 80	CC-066SS-01	X	SS	0	SC	[Hatched Pattern]	SANDY LEAN CLAY (SC): strong brown (7.5YR 4/6) 20% grades to reddish yellow (7.5YR 6/6) and 50% grades to strong brown (7.5YR 5/6), ~40% medium to coarse sand, ~60% fines, petroleum odor; odor noted at 0.9 meters bgs.		0	PVC Top Cap
1		1/3/3	0.6098 / 50				1					1	
2		2/4/4	0.6098 / 80				2	CL	[Diagonal Pattern]	CLAYEY SILT (CL): light yellowish brown (2.5Y 6/4) 60% grades to light olive brown (2.5Y 5/4), ~100% fines, petroleum odor; stiff to very stiff; odor noted at 1.8 meters bgs.		2	
3		4/6/11/15	0.6098 / 100				3					3	
4		2/6/9/12	0.3049 / 0			SS	4					4	
5		4/7/11/12	0.9146	CC-066SB-02	X		5	SC	[Dotted Pattern]	CLAYEY SAND (SC): dark reddish brown (5YR 3/2), ~70% coarse to medium sand, ~30% fines, no odor; moist; medium dense.		5	
6		5/18/22/27	0.6098 / 90				6	CC	[Cross-hatched Pattern]	CLAYEY SAND (SC): reddish yellow (5YR 7/8), ~80% coarse to medium sand, ~40% fines, no odor; moist; very dense.		6	1/2" Dia. Bentonite Pellets
7		26/31/50	0.4573 / 100				7					7	
8		5/20/38/50	0.6098				8	SC	[Dotted Pattern]	CLAYEY SAND (SC): light brown (7.5YR 6/4), ~70% coarse to medium sand, ~30% fines, moist.		8	

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41.GPJ ACE\_1836.GDT\_16/9/03

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# LOG OF WELL AREA 41 #66



PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/11/03 08:15</b>
LOGGED BY <b>[Redacted]</b>	DATE & TIME FINISHED <b>4/11/03 16:30</b>
REVIEWED BY <b>66</b>	

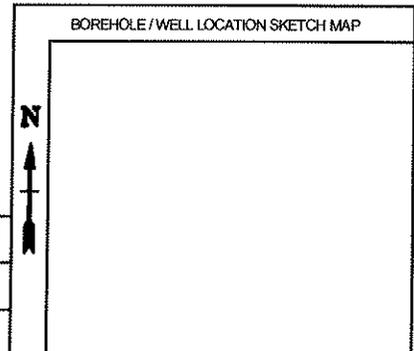
DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
10		36/44/29/40	0.9146	CC-066SB-03	X	SS	10	CL	[Hatched Pattern]	SANDY LEAN CLAY (CL): light brown (7.5YR 6/4), ~40% coarse to medium sand, ~60% fines.	10	Filter Pack
11		50	0.1524		X	SS	11	SM	[Dotted Pattern]	SILTY SAND (SM): brown (7.5YR 5/4), ~70% coarse to medium sand, ~30% fines, very dense.	11	Slotted PVC Casing
12							12			Preprobe. No recovery.	12	
14		50	0.1524				14				14	
15		100	0.1524 / 100				15	SM	[Dotted Pattern]	SILTY SAND (SM): brown (7.5YR 5/3), ~70% coarse to medium sand, ~30% fines, no odor. End of Borehole at 15.2 m.	15	Threaded PVC End Cap

BORING LOG METRIC UNITS. CAMP CARROLL AREA D AND AREA 41. GPJ ACE. 1836.GDT. 16/9/03

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# LOG OF BORING AREA 41 B-051



PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/4/03 10:10</b>		COORDINATES
LOGGED BY <b>[Redacted] b6</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/4/03 10:27</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>	DRILLING METHOD <b>Direct-Push</b>		SURFACE ELEVATION <b>mean sea level</b>
SAMPLING METHOD <b>Geoprobe Sampler</b>	SAMPLE HAMMER TYPE	SIZE / TYPE OF BIT	

WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	CASING MATERIAL / DIAMETER	SCREEN Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING
		TOP & BOTTOM OF SCREEN
		PRODUCT SURFACE
		GROUNDWATER SURFACE
		DATE

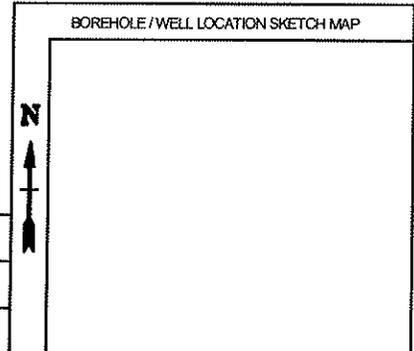
DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
			0.9 / 80 0.4	SS051SS0	X	SS		SC		CLAYEY SAND (SC): strong brown (7.5YR 5/6), ~5% gravel, ~55% fine to coarse sand, ~40% fines, moist; dense; fill soil.		NO WELL INSTALLED	
								CL		LEAN CLAY (CL): dark grayish brown (10YR 4/3), ~100% fines, medium to high, moist; stiff.			
			1.3 / 80					SC		CLAYEY SAND (SC): yellowish brown (10YR 5/6), ~55% fine to medium sand, ~45% fines, moist; dense.			
										End of Borehole at 2.3 m.			

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41, GPJ, ACE, 183E, GET, 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF BORING AREA 41 B-052



PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/3/03 13:30</b>		
LOGGED BY <b>[Redacted] b6</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/3/03 14:05</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>	DRILLING METHOD <b>Direct-Push</b>	COORDINATES	
SAMPLING METHOD <b>Geoprobe Sampler</b>	SAMPLE HAMMER TYPE	SIZE / TYPE OF BIT	SURFACE ELEVATION <b>mean sea level</b>
WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	CASING MATERIAL / DIAMETER	SCREEN	Type: Material: Length: Diameter: Slot Size:

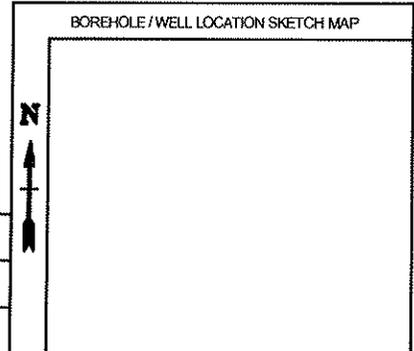
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE
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DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
0			1 / 70			SS	0	SC	[Hatched Pattern]	CLAYEY SAND (SC): ( 7.5YR 4.5/6), ~60% fine to coarse sand, ~40% fines, moist; dense.		0	NO WELL INSTALLED
1			1.3	CC052SS0			1	SC	[Hatched Pattern]	CLAYEY SAND (SC): strong brown (7.5YR 5/6), ~60% fine to coarse sand, ~40% fines, moist; more friable.		1	
2			1.5 / 70				2					2	
3			0.5 / 90				3			Refusal. End of Borehole at 3.0 m.		3	
4							4					4	
5							5					5	
6							6					6	
7							7					7	
8							8					8	

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41.GPJ ACE. 1836.GDT 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF BORING AREA 41 B-055

PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/4/03 10:00</b>		COORDINATES
LOGGED BY <b>[Redacted] b6</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/4/03 10:09</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>	DRILLING METHOD <b>Direct-Push</b>		SURFACE ELEVATION <b>DATUM mean sea level</b>
SAMPLING METHOD <b>Geoprobe Sampler</b>	SAMPLE HAMMER TYPE	SIZE / TYPE OF BIT	

WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	CASING MATERIAL / DIAMETER	SCREEN Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____				
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE

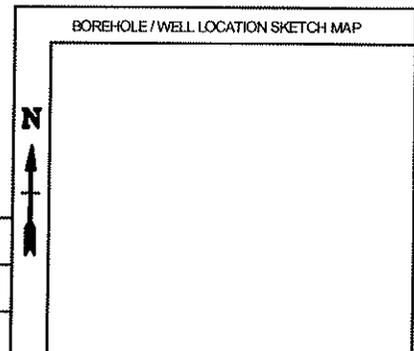
DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
			0.7 / 80				0	CL		SANDY LEAN CLAY (CL): red (2.5YR 4/6), ~30% fine to medium sand, ~70% fines, low, moist; firm; fill soil.			NO WELL INSTALLED
			1.5 / 60				1	SC		CLAYEY SAND (SC): yellowish brown (10YR 5/6), ~55% fine to medium sand, ~45% fines, moist; dense.			
							2.3			End of Borehole at 2.3 m.			

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41 GPJ ACE\_183E.GDT 16/9/03

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# LOG OF BORING AREA 41 B-056



PROJECT NO.		PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>	
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>		DATE & TIME STARTED <b>4/4/03 09:45</b>	
LOGGED BY <b>[Redacted] b6</b>		DATE & TIME FINISHED <b>4/4/03 09:57</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>		DRILLING METHOD <b>Direct-Push</b>	
SAMPLING METHOD <b>Geoprobe Sampler</b>		COORDINATES	
WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>		SURFACE ELEVATION DATUM <b>mean sea level</b>	

CASING MATERIAL / DIAMETER		SCREEN	
Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____			
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN
			PRODUCT SURFACE
			GROUNDWATER SURFACE
			DATE

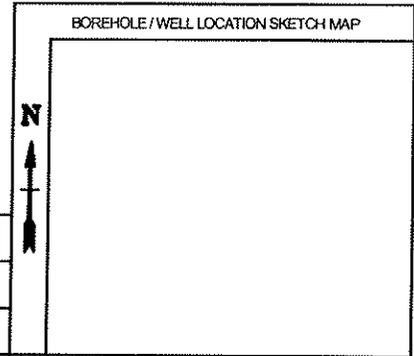
DEPTH (meters bgs)	PtD (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
			0.7 / 80	CC056SS01	X	SS		SC	[Hatched Pattern]	CLAYEY SAND (SC): yellowish brown (10YR 5/6), ~55% fine to medium sand, ~45% fines, moist; dense.			NO WELL INSTALLED
			1.5 / 80					SC	[Hatched Pattern]	CLAYEY SAND (SC): strong brown (7.5YR 4.5/6), ~55% fine to medium sand, ~45% fines, moist; dense.			
										End of Borehole at 2.3 m.			

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41 (PJ) ACE 1835.GCT 16/9/03

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF BORING AREA 41 B-057



PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 R1</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/4/03 10:30</b>		
LOGGED BY <b>[Redacted]</b>	REVIEWED BY <b>bc</b>	DATE & TIME FINISHED <b>4/4/03 10:40</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>	DRILLING METHOD <b>Direct-Push</b>	COORDINATES	
SAMPLING METHOD <b>Geoprobe Sampler</b>	SAMPLE HAMMER TYPE	SIZE / TYPE OF BIT	SURFACE ELEVATION <b>mean sea level</b>

WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	CASING MATERIAL / DIAMETER	SCREEN Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____				
ELEVATION OF (msl)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN	PRODUCT SURFACE	GROUNDWATER SURFACE	DATE

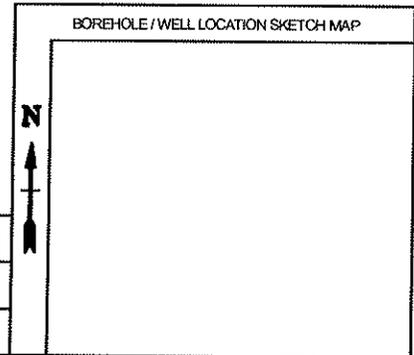
DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION		
0.7		80	1.2	CC057SS0		SS		SC		CLAYEY SAND (SC): strong brown (7.5YR 5/6), ~55% fine to medium sand, ~45% fines, moist, dense.	NO WELL INSTALLED	
1.1		80								End of Borehole at 2.0 m.		

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41 (PJ ACE 1835.GIT 16/9/03)

This log is part of the report prepared for the named project and should be read together with that report for complete information. This summary applies only at the location of this boring / well and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented is a simplification of actual conditions encountered.

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# LOG OF BORING AREA 41 B-058



PROJECT NO.		PROJECT NAME <b>Camp Carroll Area D and Area 41 RI</b>	
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>		DATE & TIME STARTED <b>4/4/03 09:25</b>	
LOGGED BY <b>[Redacted]</b>		DATE & TIME FINISHED <b>4/4/03 09:40</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>		DRILLING METHOD <b>Direct-Push</b>	
SAMPLING METHOD <b>Geoprobe Sampler</b>		COORDINATES	
WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>		SURFACE ELEVATION DATUM <b>mean sea level</b>	
ELEVATION OF (msl)		SCREEN Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____	
WELL COVER		TOP & BOTTOM OF SCREEN	
TOP OF WELL CASING		PRODUCT SURFACE	
		GROUNDWATER SURFACE	
		DATE	

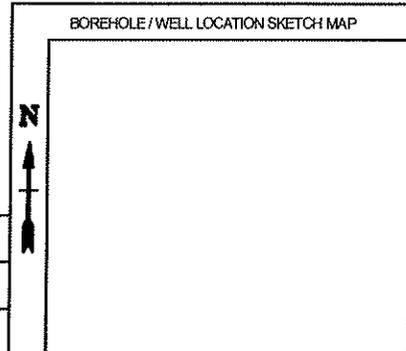
BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41, GPJ ACE 1836 GDT 16/9/03

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:	DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
			0.7 / 80			SS		CL		SANDY LEAN CLAY (CL): red (2.5YR 4/6), ~30% fine to medium sand, ~70% fines, low, moist; firm; fill soil.		NO WELL INSTALLED
1			0.6	CC058SS01		SS		SC		CI AVEY SAND (SC): yellowish brown (10YR 5/6), ~55% fine to medium sand, ~45% fines, moist; dense.		
2			1.4 / 80	CC058BS01		SS						
3										End of Borehole at 2.4 m.		
4												
5												
6												
7												
8												

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# LOG OF BORING AREA 41 B-059



PROJECT NO.	PROJECT NAME <b>Camp Carroll Area D and Area 41 Ri</b>		
LOCATION <b>Camp Carroll, Taegu, Republic of Korea</b>	DATE & TIME STARTED <b>4/4/03 10:50</b>		COORDINATES
LOGGED BY <b>[Redacted] bl</b>	REVIEWED BY	DATE & TIME FINISHED <b>4/4/03 11:05</b>	
DRILLING CONTRACTOR / DRILLER <b>Beautiful Environmental Corp</b>	DRILLING METHOD <b>Direct-Push</b>	SURFACE ELEVATION <b>mean sea level</b>	
SAMPLING METHOD <b>Geoprobe Sampler</b>	SAMPLE HAMMER TYPE	SIZE / TYPE OF BIT	DATUM

WELL INSTALLED? YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	CASING MATERIAL / DIAMETER	SCREEN	Type: _____ Material: _____ Length: _____ Diameter: _____ Slot Size: _____
ELEVATION OF (mst)	WELL COVER	TOP OF WELL CASING	TOP & BOTTOM OF SCREEN
			PRODUCT SURFACE
			GROUNDWATER SURFACE
			DATE

DEPTH (meters bgs)	PID (ppmv)	BLOWS / DRIVE	DRIVE / RECOVERY (meters / %)	LAB SAMPLE ID	EXTENT	SAMPLE TYPE	DEPTH (meters bgs)	USCS	GRAPHIC LOG	SURFACE CONDITION:		DEPTH (meters bgs)	WELL CONSTRUCTION DETAILS
										LITHOLOGIC DESCRIPTION			
			0.7 / 80			SS		SC	[Hatched Pattern]	CLAYEY SAND (SC); strong brown (7.5YR 5/6), ~60% fine to coarse sand, ~40% fines, moist; dense; fill soil.			NO WELL INSTALLED
			1.5	CC059SS0				SC	[Hatched Pattern]	CLAYEY SAND (SC); strong brown (7.5YR 5/6), ~55% fine to medium sand, ~45% fines, moist; dense.			
			1.6 / 80							End of Borehole at 2.4 m.			

BORING LOG METRIC UNITS CAMP CARROLL AREA D AND AREA 41 (SPJ ACE\_183E.GIT\_16/9/03)

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